

S & T treat baluns on pp. 180-187,
Sect. 5.3 "Feeding Wire Antennas"
(read this!)

Kraus treats "matching problems" on
pp. 734-745. Discussion on baluns
is mostly contained on pp. 741-745,
Sect. 16.11.

16-2

Balanced to Unbalanced transformers

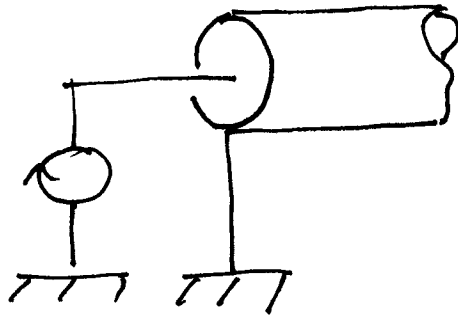
or BALUNS

Why needed?

What are they?

How do they work?

Most typical example of an unbalanced system is coaxial cable.



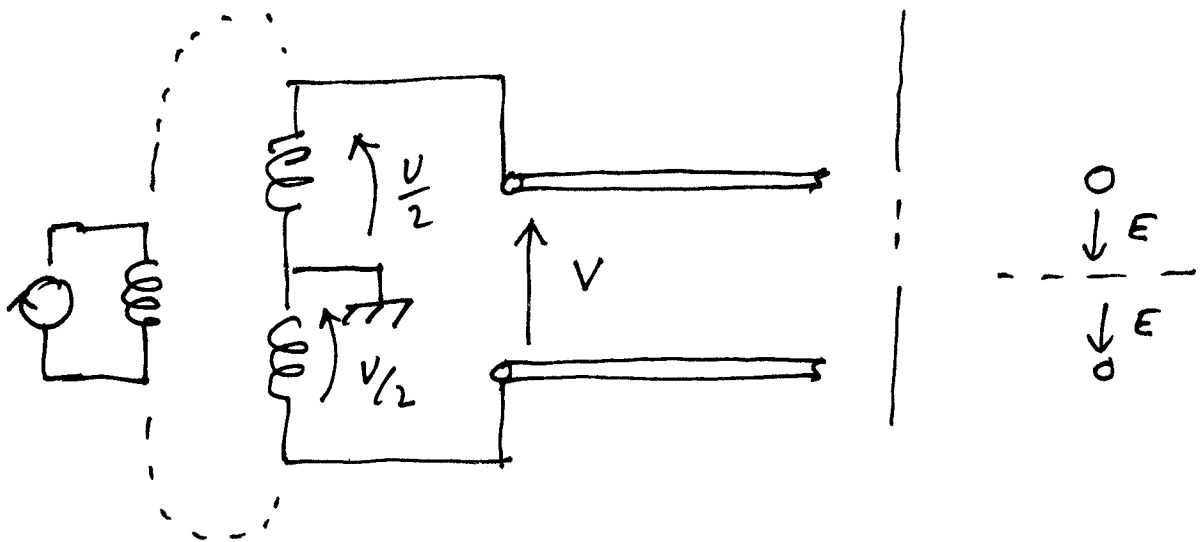
Unbalanced because all potentials are of same sign* w.r.t reference potential "0"

(instantaneously, at a given location)

1...

16-4

Contrast this with



Symmetrical w.r.t. 0, said to be

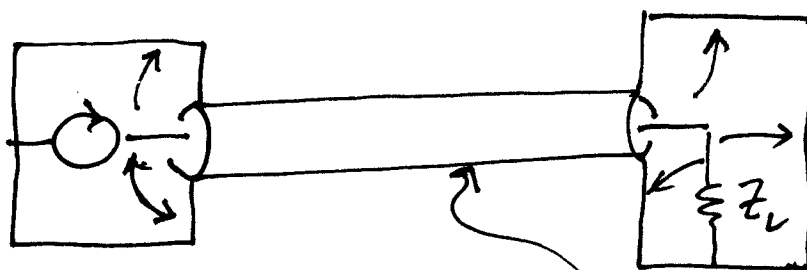
But some antennas are "balanced,"
while others are "unbalanced."

How to connect balanced and
unbalanced systems?

16-6

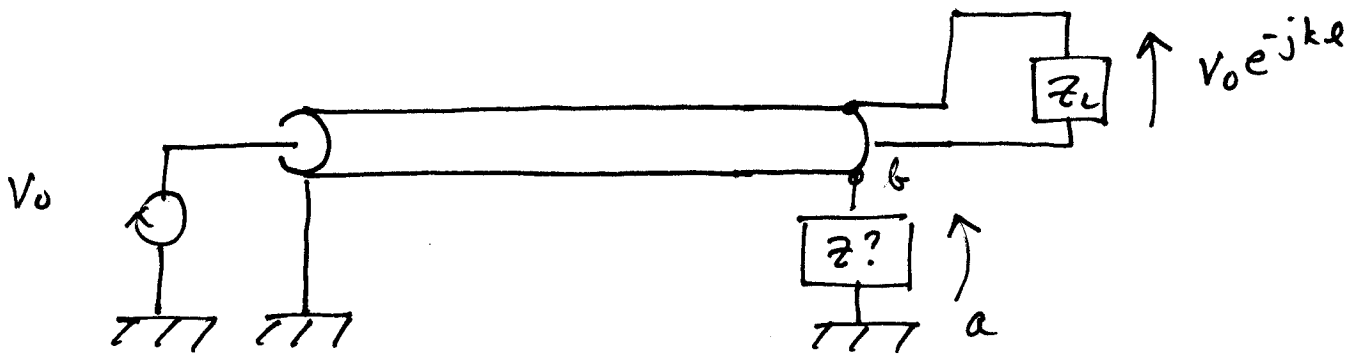
Unbalanced Systems occur "naturally" - in
active devices, e.g.

They can be completely shielded



Coaxial Line

Consider,



$$V_{ab} = \int_a^b \vec{E} \cdot d\vec{s} = \int_a^b (-\nabla\phi - j\omega\mu\vec{A}) \cdot d\vec{s}$$

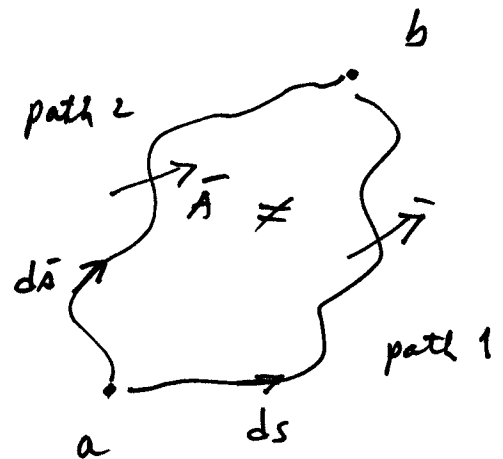
$$= - \int_a^b \nabla\phi \cdot d\vec{s} - j\omega\mu \int_a^b \vec{A} \cdot d\vec{s}$$

/...

16-8

$$V_{ab} = \underbrace{\phi_a - \phi_b}_{=0} - j\omega\mu \int_a^b \vec{A} \cdot d\vec{s} \neq 0$$

$\nabla\phi$ is conservative field
 $= 0$ when integrated
 around a loop.

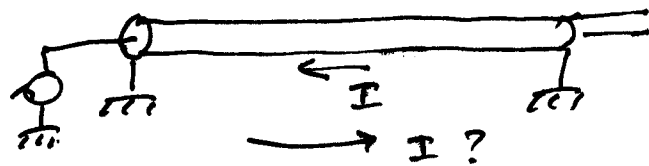


$$V_{ca} = 0 - j\omega\mu \int_a^a \vec{A} \cdot d\vec{s}$$

$$= -j\omega\mu \int \nabla \times \vec{A} \cdot d\vec{s}$$

$\int_a^b \vec{A} \cdot d\vec{s}$ depends on path of

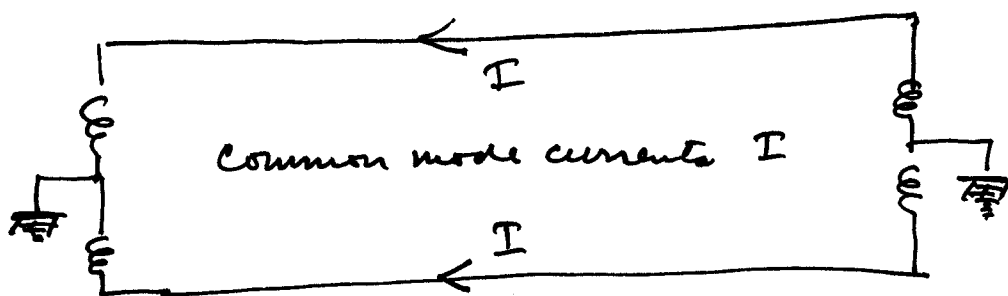
So, in the presence of \bar{A} (or \bar{B}), external to a coaxial conductor, currents can flow on the outside of the outer conductor as the result of "induction." That is, induced potential differences on different parts of the conductor result in currents necessary to maintain $\bar{E}_{\text{tang}} = 0$. Since $V_{aa} \neq 0$, this can occur even when the conductor (the outer coaxial braid, e.g.) appears to be "grounded."

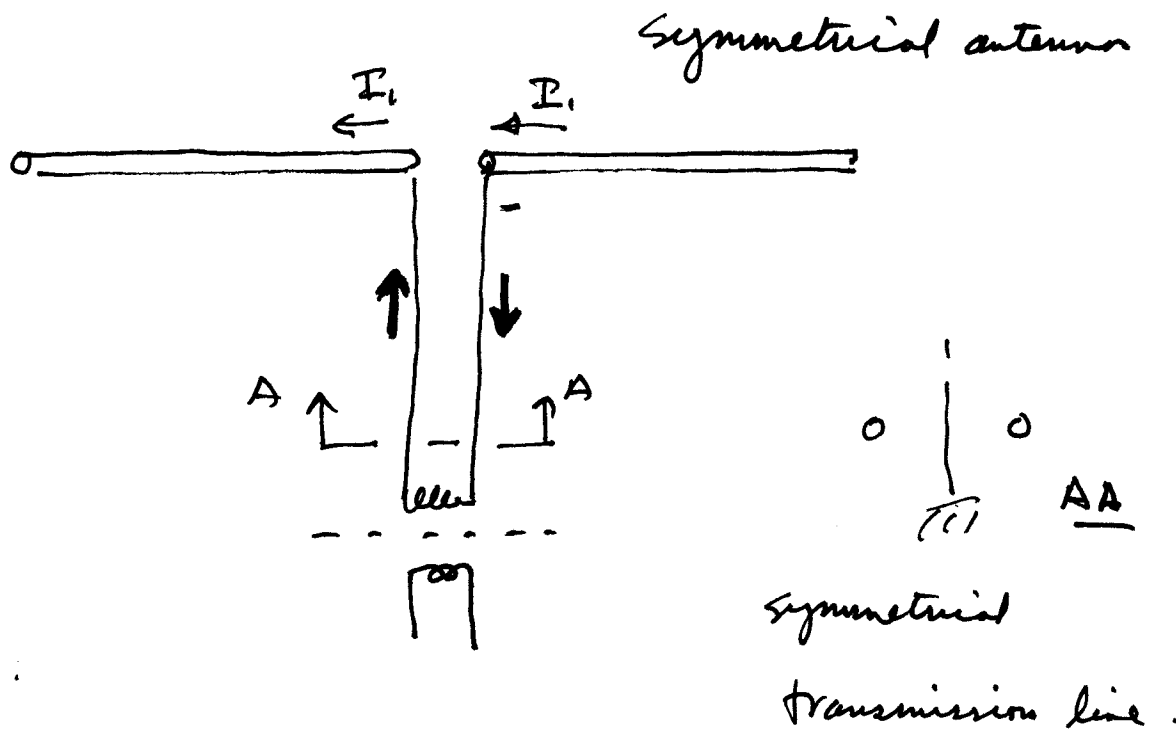


16-10

N.B. The circuit need not close through an external connection, however.

Aside: Similar phenomena can occur on balanced lines.



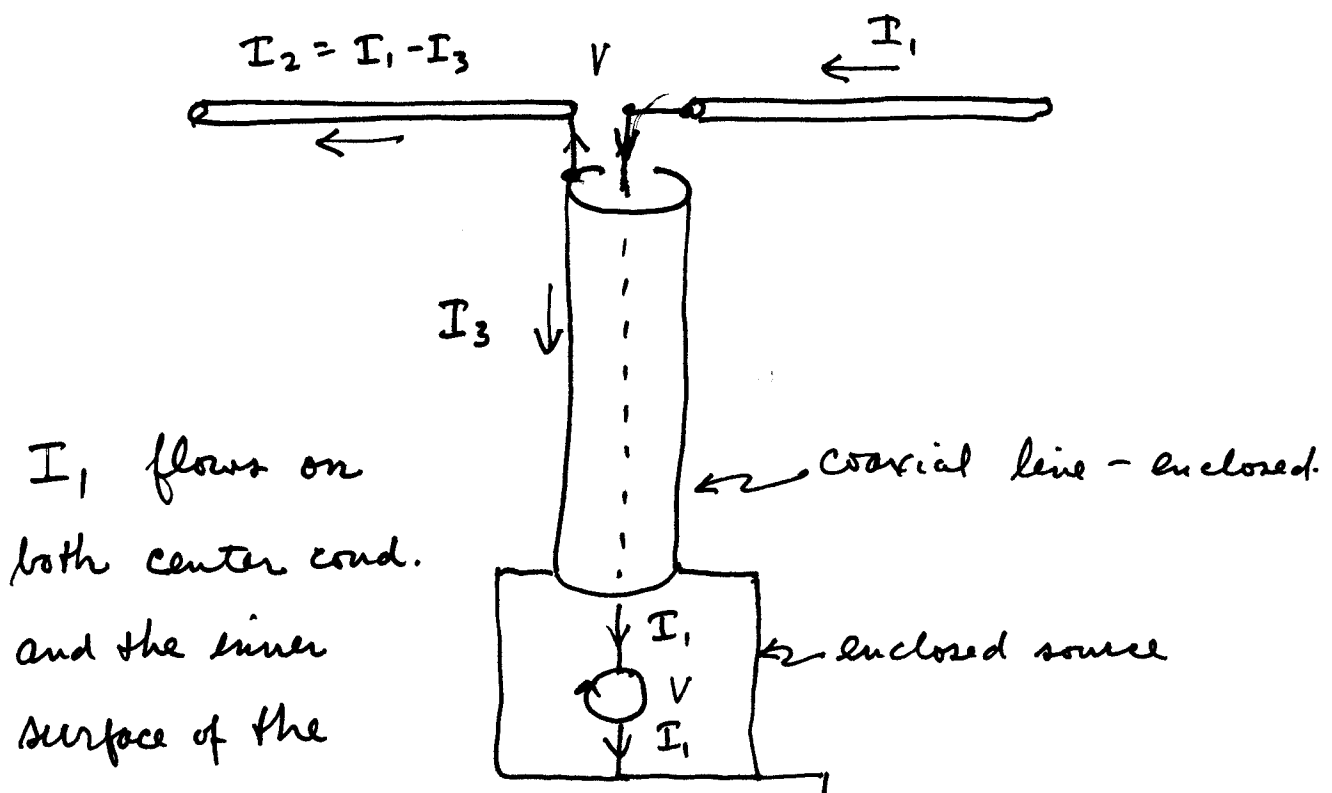


Balanced system

No Problem

Symmetrical Antenna - Unbalanced Line

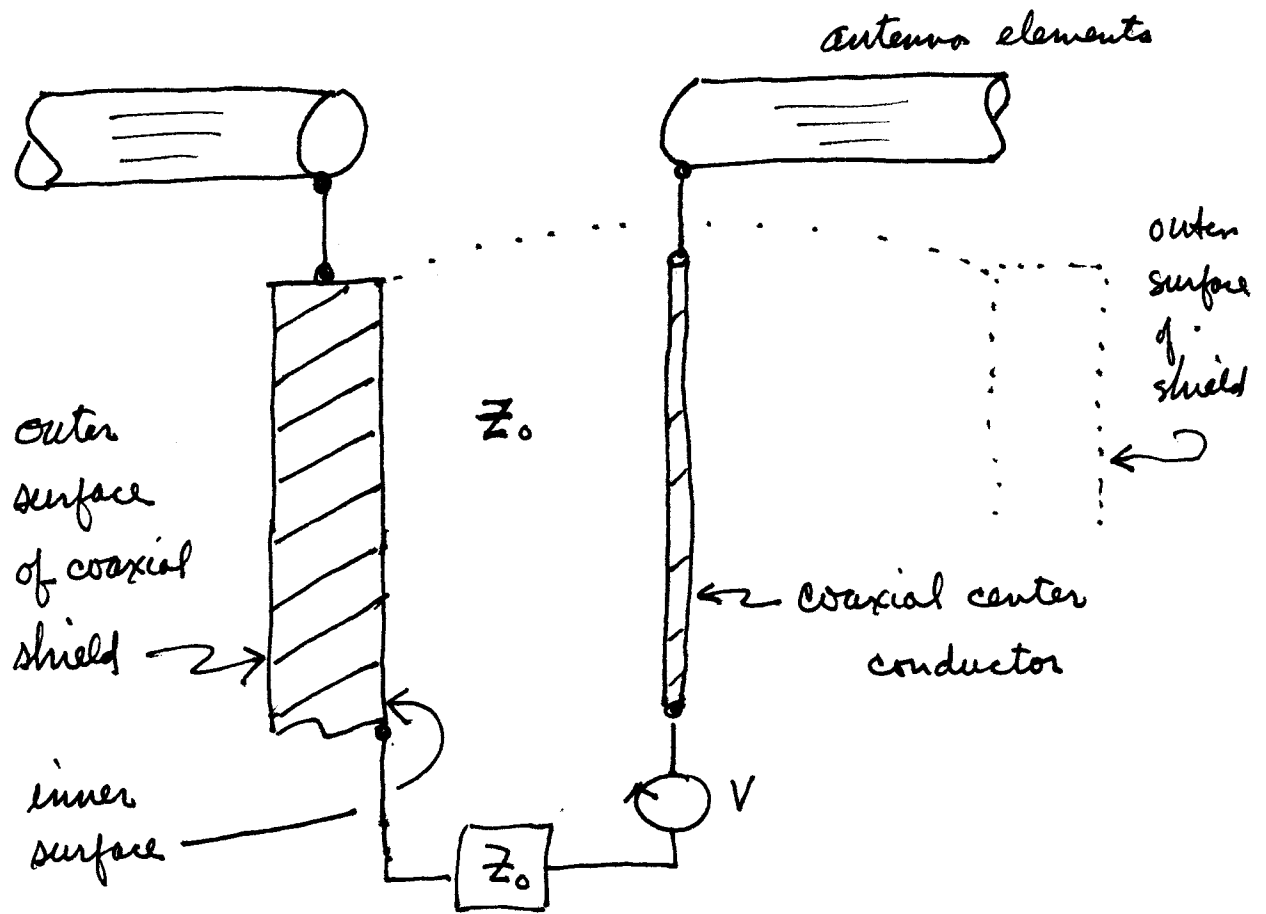
16-12



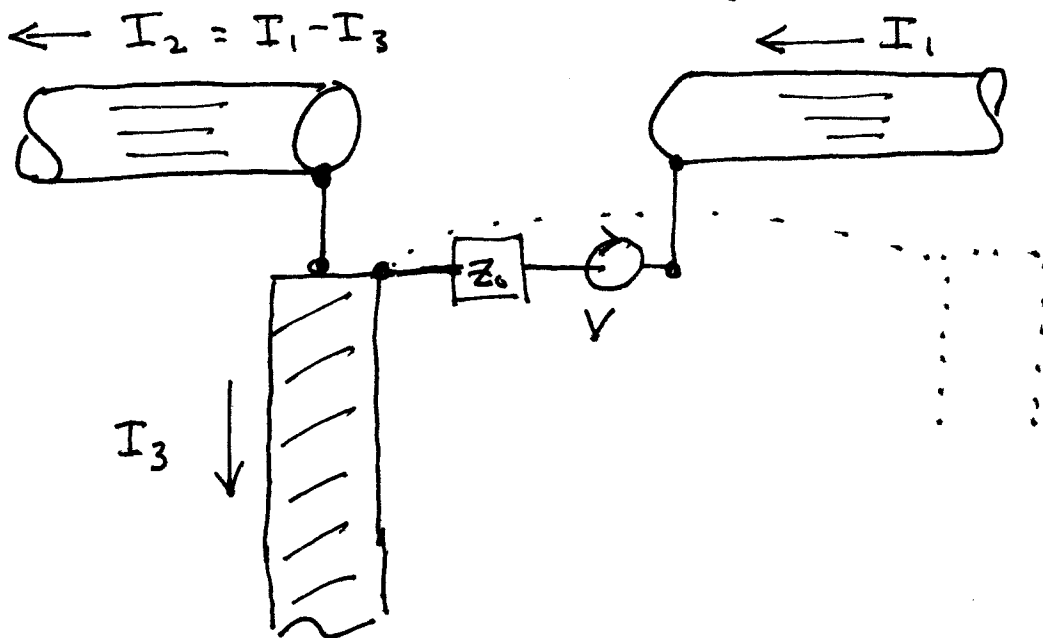
I_1 flows on both center cond. and the inner surface of the

Here is an snappier sketch of the situation:

at the antenna feed point...

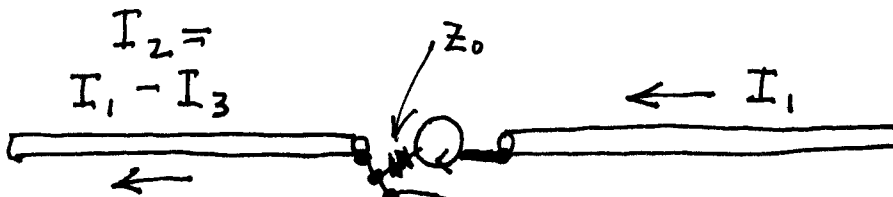


Owing to the properties of a matched transmission line this is equivalent to...



Another way to think of this —

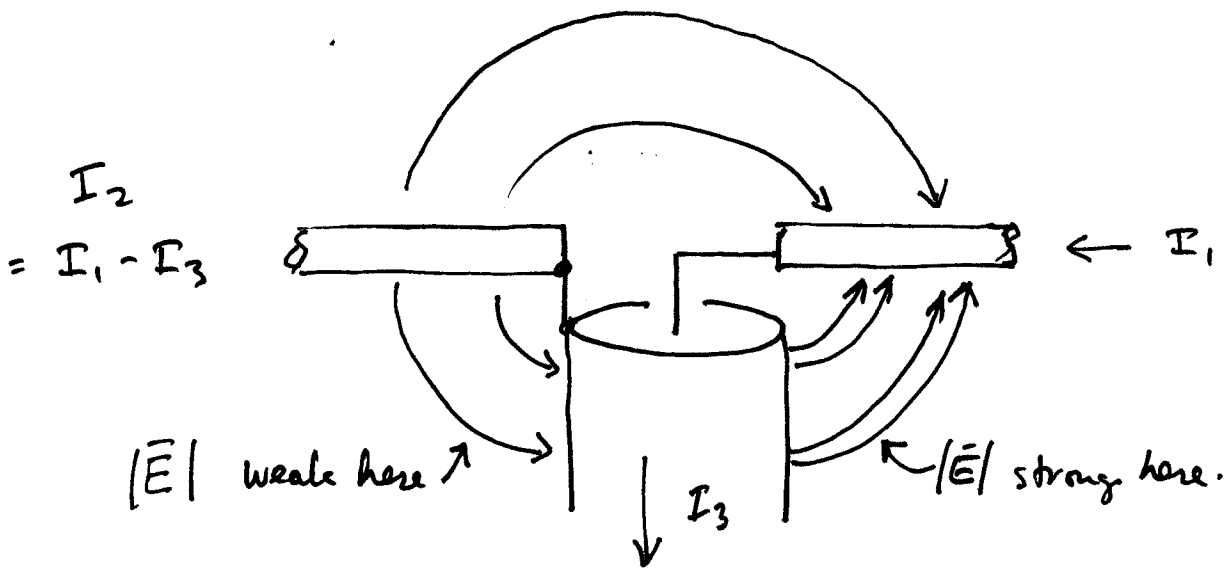
At the feed point we have, in effect...



I_3 will depend (typically) on unknown, uncontrolled factors in the vicinity of the equipment.

Current division between I_2, I_3 depends on the impedance presented to the source.

16-16



Why?

Radiation results from I_1, I_2, I_3

$I_1 \neq I_2, I_3 \neq 0$ corrupts pattern and

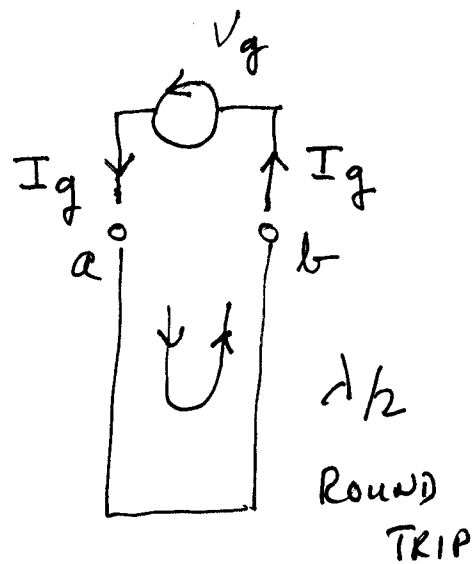
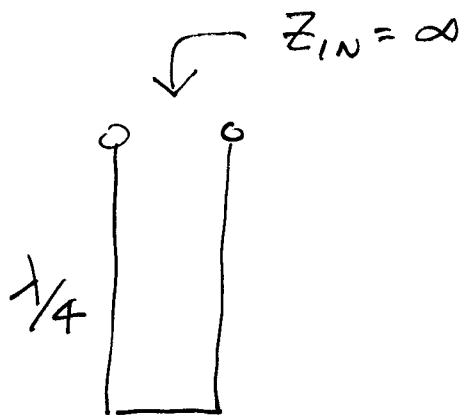
Pattern problems important for both transmitting and receiving.

Uncontrolled flow of currents is (or can be) dangerous in high power equipment.

16-18

How to BLOCK I_3 ?

CONSIDER

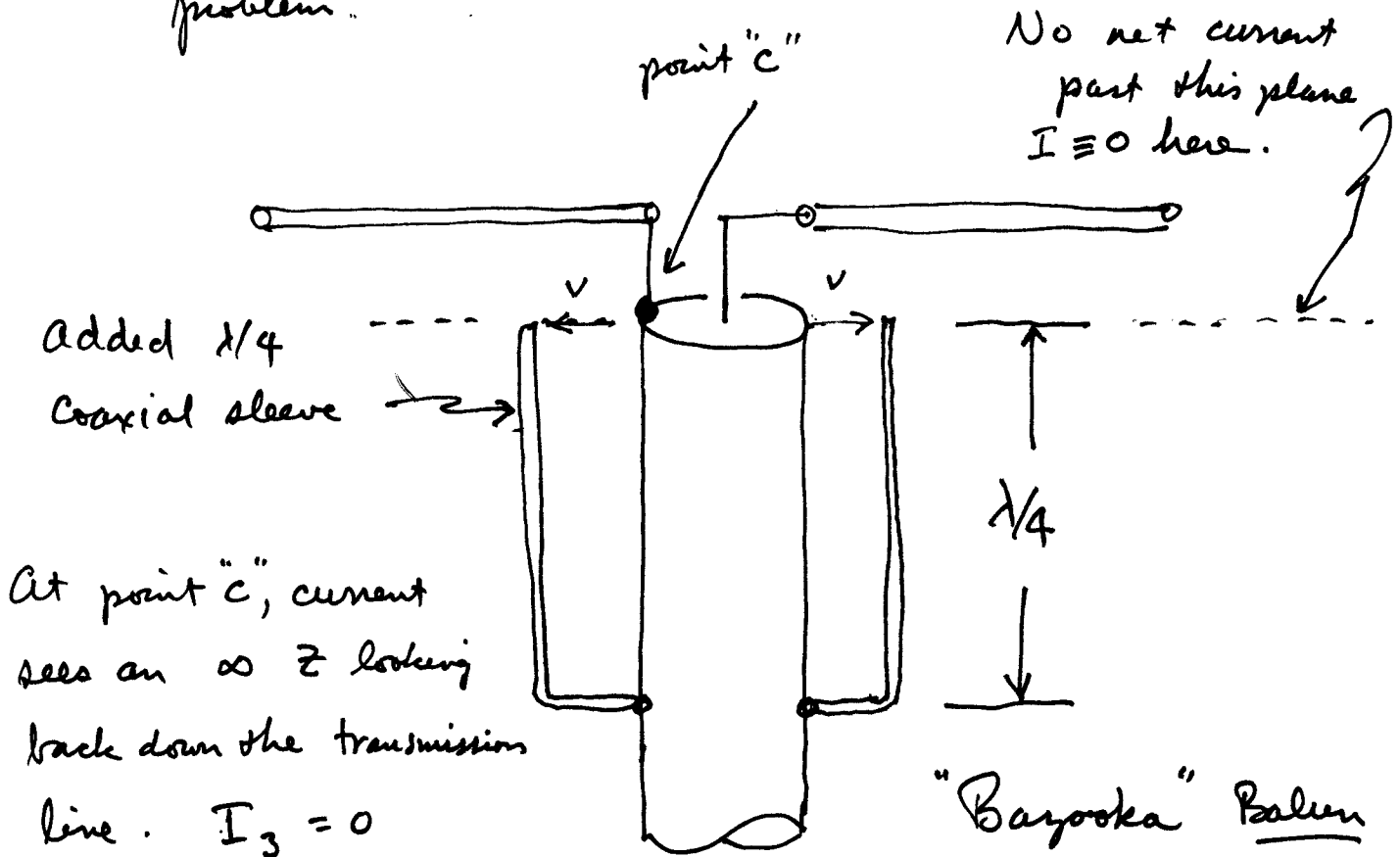


WHEN PHASE REVERSAL IS CONSIDERED

$\lambda/2$ path from $a \rightarrow b$ and vice versa cancels I_g at feed point!

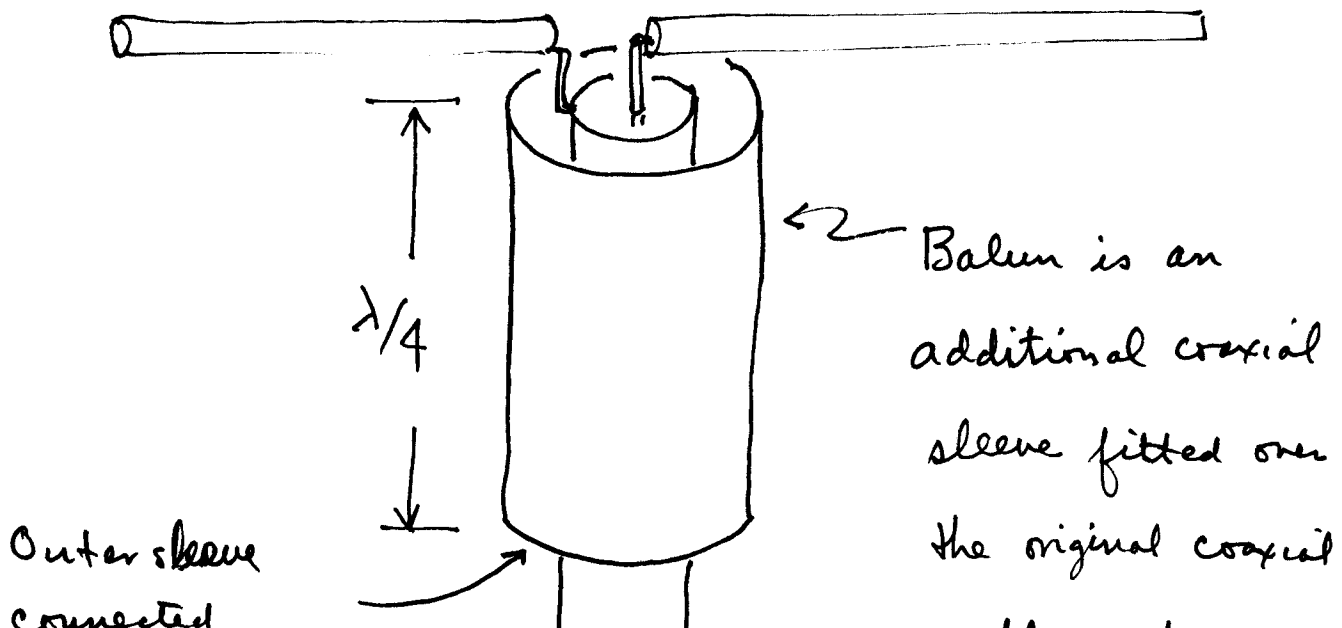
$\lambda/4$ transformer can be applied to antenna

problem.

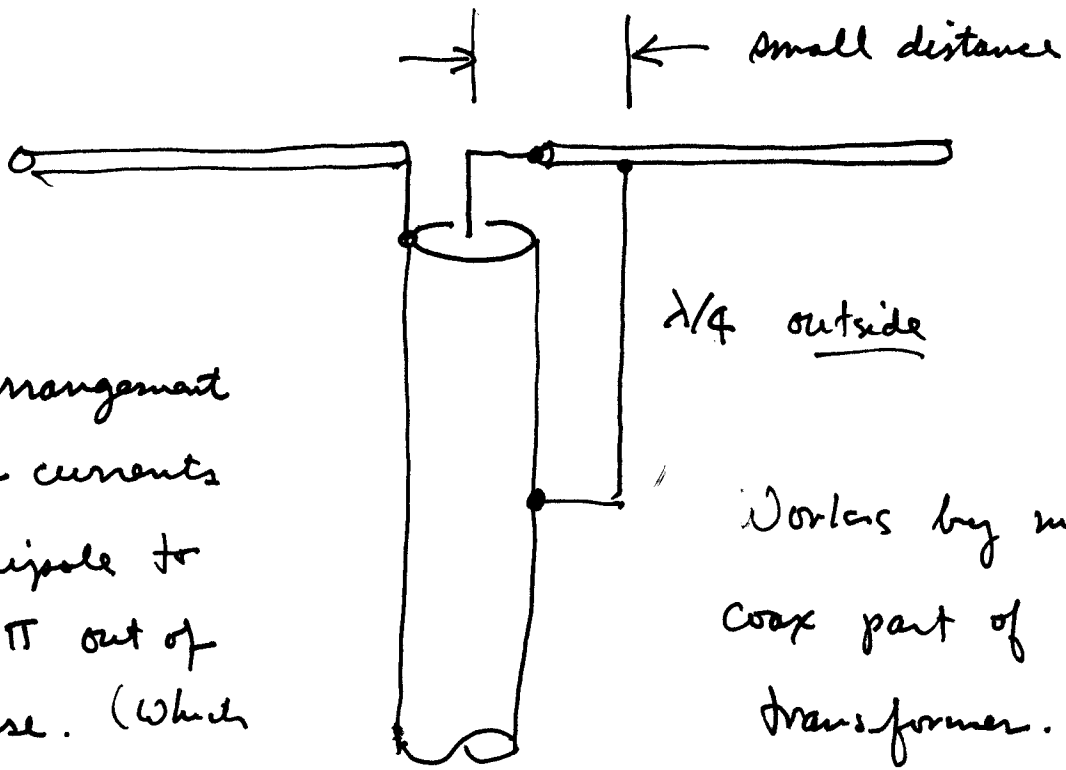


16-20

Perspective View of the Bazooka Balun



Alternative

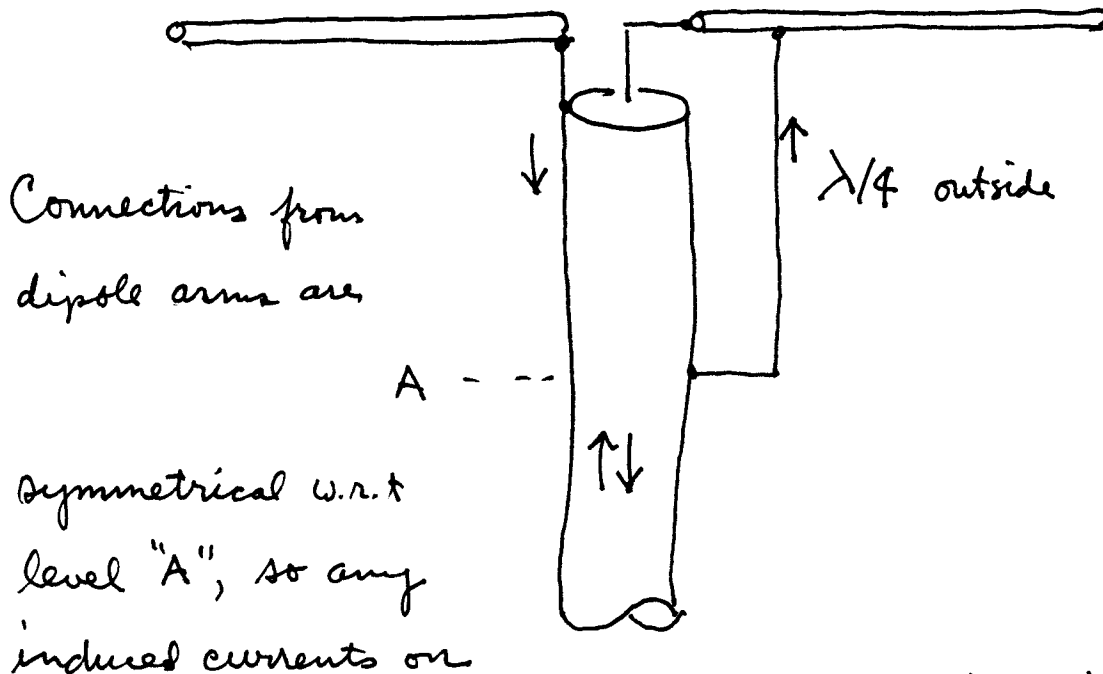


This arrangement forces currents on dipole to be π out of phase. (Which means in phase in our context!)

Works by making coax part of $\lambda/4$ transformer.

Called 1:1 Balun

16.22

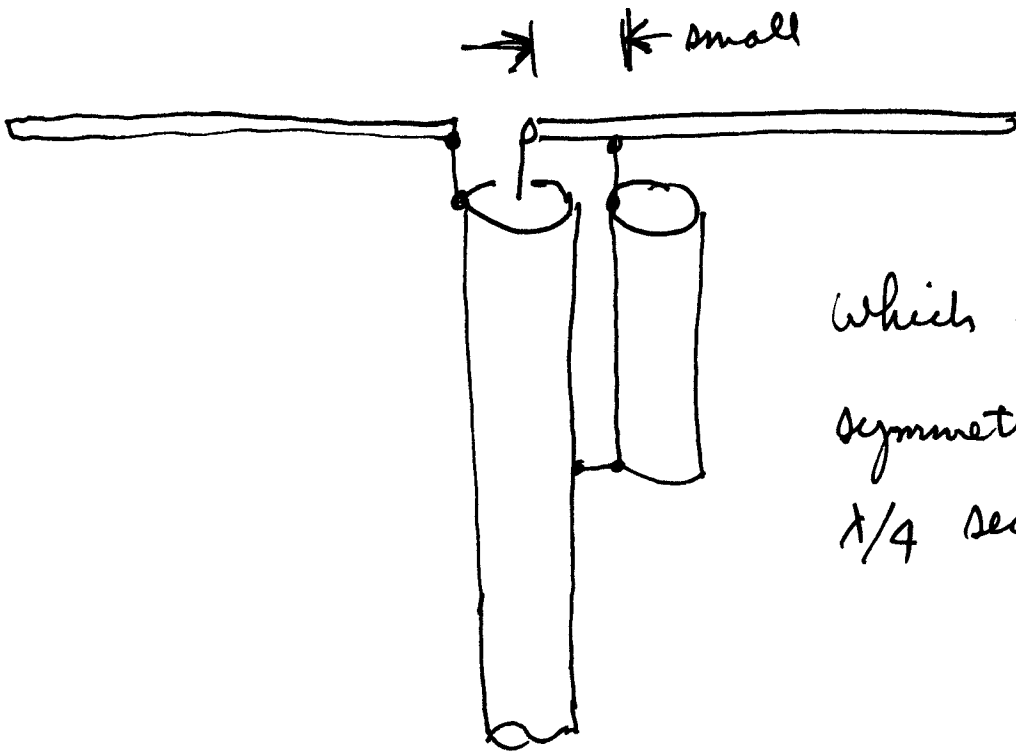


Connections from dipole arms are

A - - -

symmetrical w.r.t level "A", so any induced currents on

1:1 Balun sometimes realized as ...

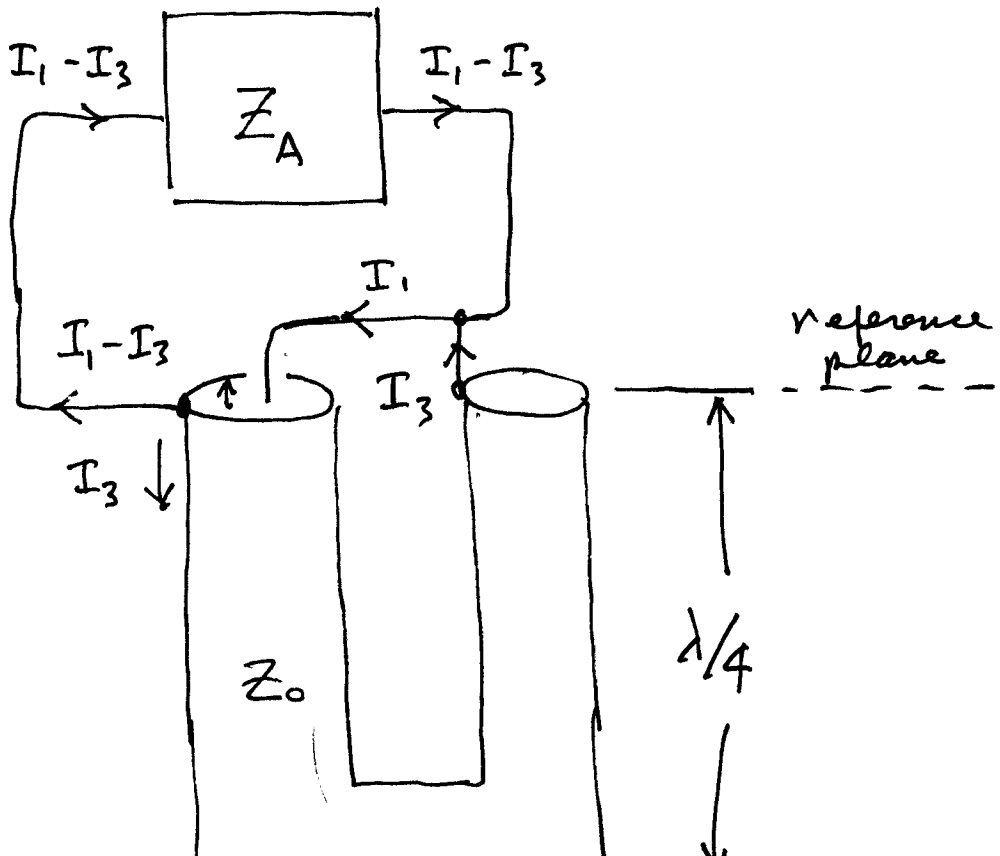


Which gives better symmetry in the $\lambda/4$ section.

What about 1:1 Balun? (For match $Z_A = Z_0$)

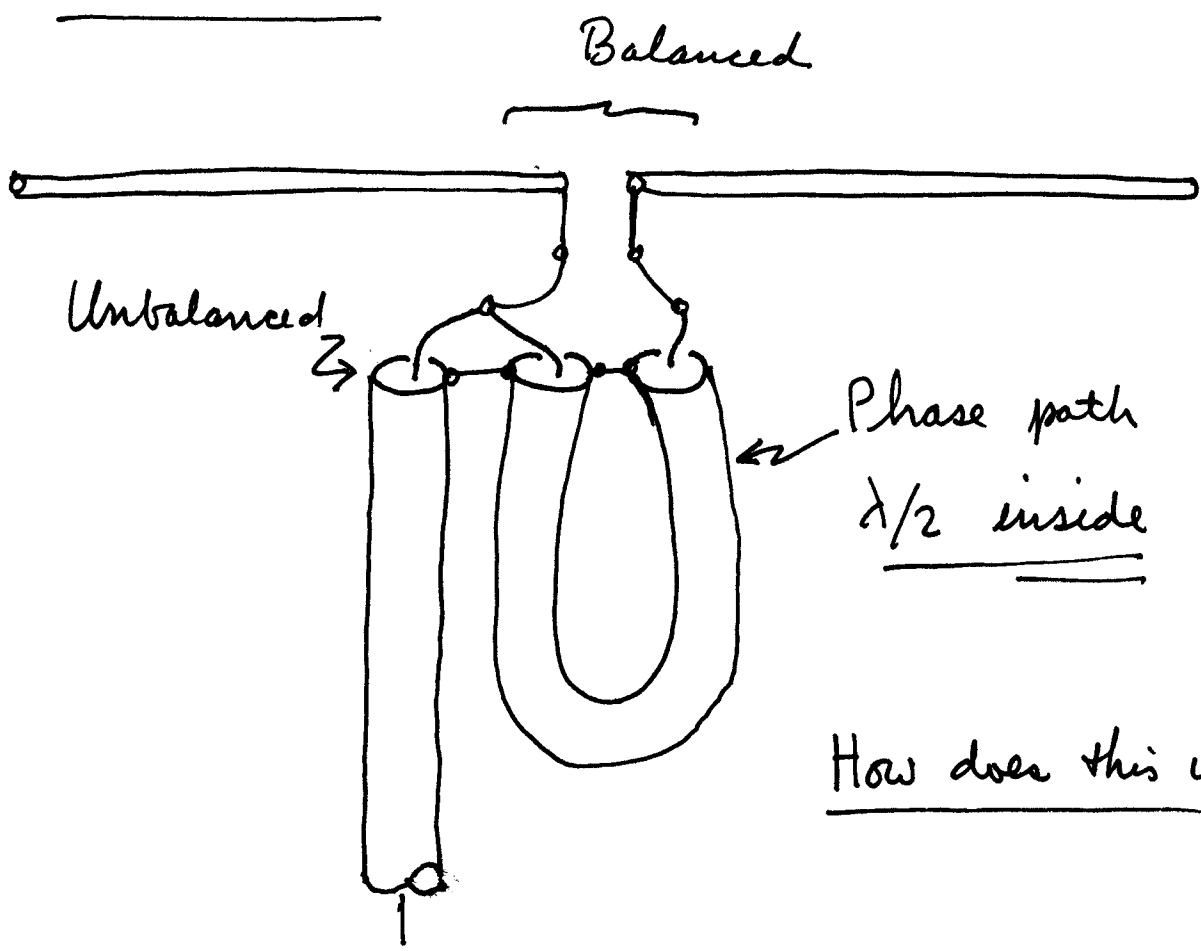
16-24

A. No net current can pass down the line beyond the $\lambda/4$ section



B. $I_3 = 0$ because $\lambda/4$ section is ∞Z at

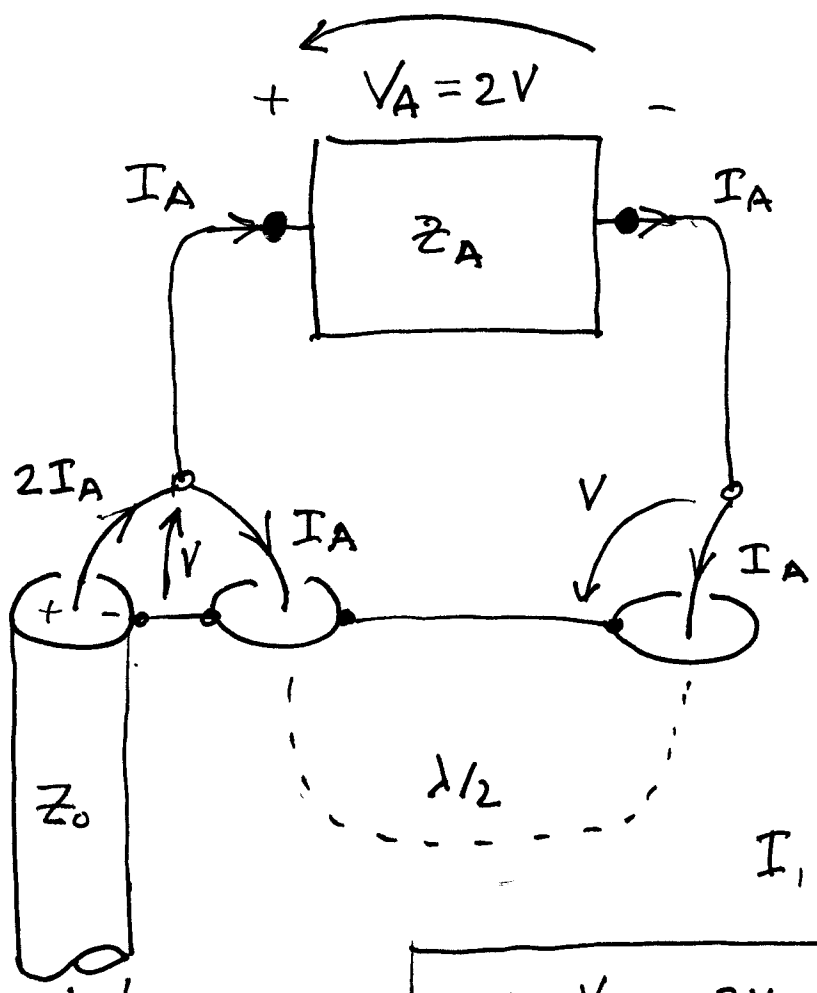
4.1 Balun



How does this work??

16-26

$Z_0 = \frac{V}{I}$



Currents on antenna elements are forced to be equal (I_A) by $\lambda/2$ phasing

I, V reverse in $\lambda/2$

$Z' = \frac{V_A}{I_A} = \frac{2V}{I_A} = 4 Z_0$

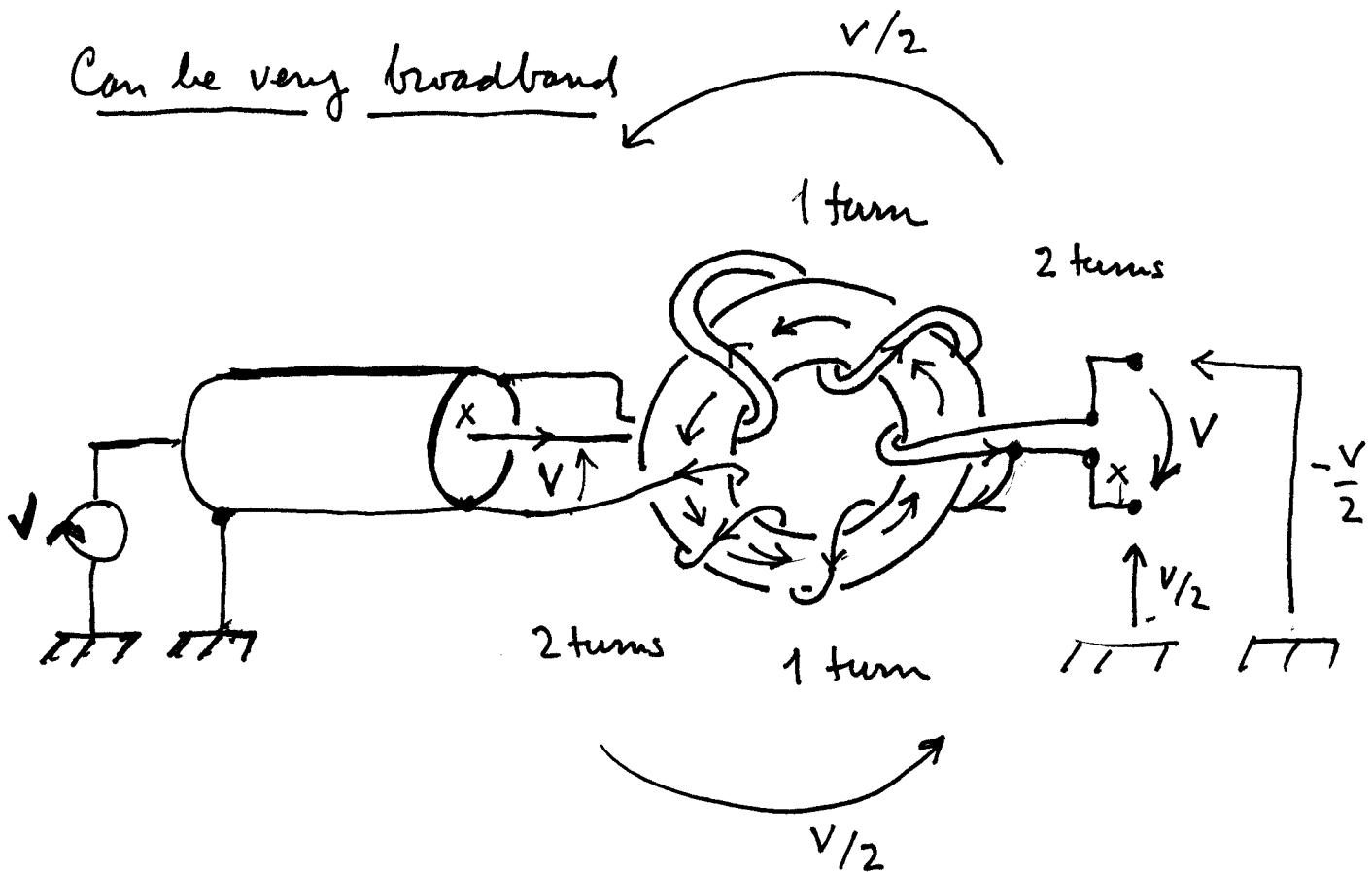
They are all narrow band. (They depend on specific phasing structures implemented w/ transmission lines.

Broad band solutions can be realized w/ circuit type elements.

See below

1..

16-28



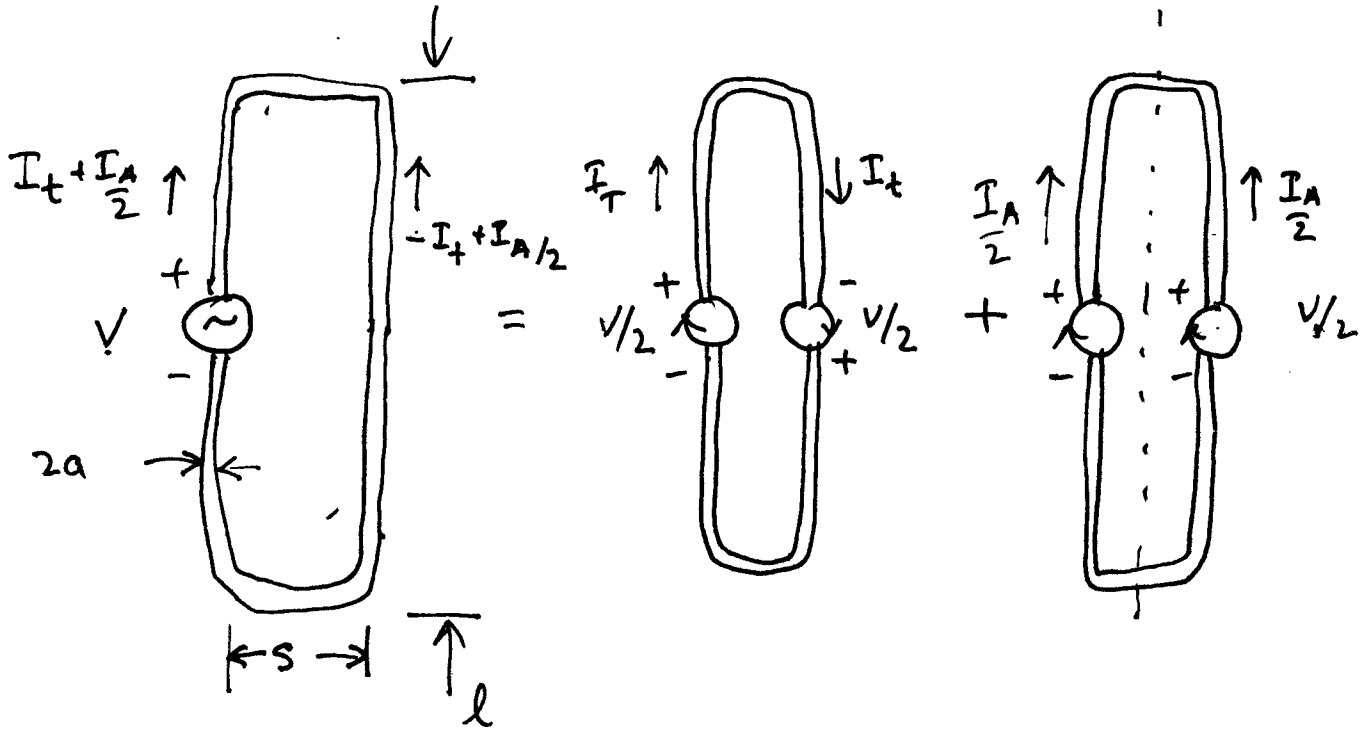
Non-linear \rightarrow harmonics

Lossy

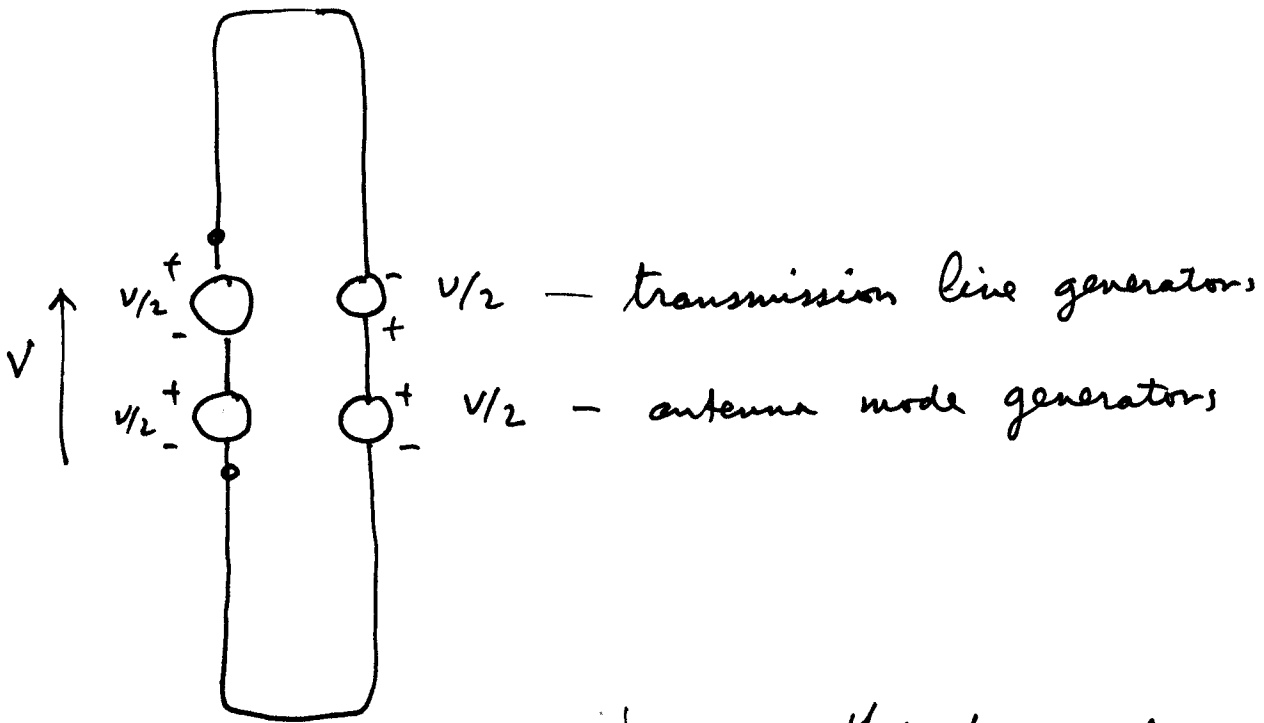
Other examples of Z transformation.

Folded Dipole

$s, 2a \ll l, l \approx \lambda/2$



16-30

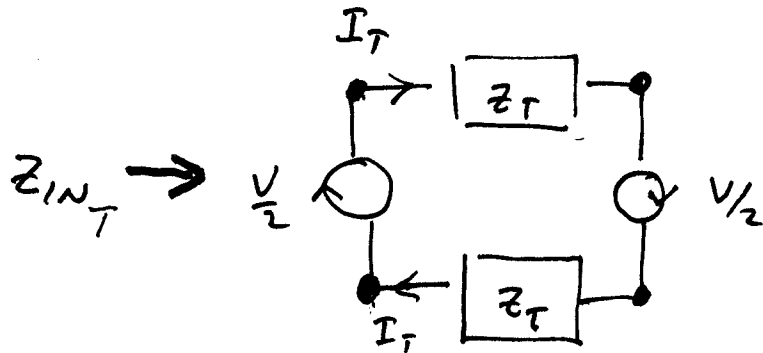


How can this be analyzed?

Use superposition!

For transmission line mode $Z_T = j Z_0 \tan[\beta l/2]$

An equivalent circuit is



$$Z_{IN_T} = ? \quad I_T = \frac{2 \cdot V/2}{2 Z_T} = \frac{V}{2 Z_T}$$

$$Z_{IN_T} = \frac{V}{I_T} = 2 Z_T$$

16-32

For antenna mode, I_A is approximately that of a single dipole with excitation $V/2$

$$I_A \approx \frac{V/2}{Z_D} = \frac{V}{2 Z_D}; \quad Z_D = \text{dipole input impedance}$$

$$Z_{IN_D} \approx \frac{V}{I_A} = 2 Z_D$$

Input Z doubled! Why? Voltage required to drive a given current is doubled by close

So what is input Z for the whole thing?

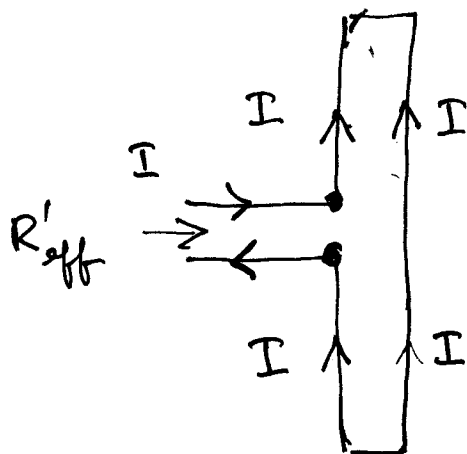
$$Z_{in} \approx \frac{V}{I_T + \frac{1}{2} I_A} = \frac{V}{\frac{V}{2Z_T} + \frac{1}{2} \frac{V}{2Z_D}} = \frac{4Z_T Z_D}{2Z_D + Z_T}$$

$Z_{in} \rightarrow 4Z_D$
 when $Z_T \rightarrow \infty$,
 which occurs when $l \approx \lambda/2$

So input impedance
 is quadrupled!

16-34

An alternative view, valid at resonance is as follows:



Effective radiating current is $2I$, so the radiated power has increased by $\times 4$.

$$\underbrace{\frac{1}{2} R'_{eff} I_{\Sigma}^2}_{\text{folded dipole}} = \underbrace{4 \cdot \frac{1}{2} R_{eff} I^2}_{4 \times \text{simple dipole}}$$

$$R'_{eff} = 4 \cdot R_{eff}$$

Summary - for Folded Dipole

$$Z_{in} \approx 4 Z_D \quad (l = \lambda/2)$$

$$Z_{in} \approx 4(73 + j42) = 292 + j168 \Omega$$

Resonate this by trimming, $Z_{in} \approx 300 \Omega$,
which matches 300Ω twin line.

Such dipoles generally are more broadband
than straight dipoles. Why?? Think about
this.

16-36

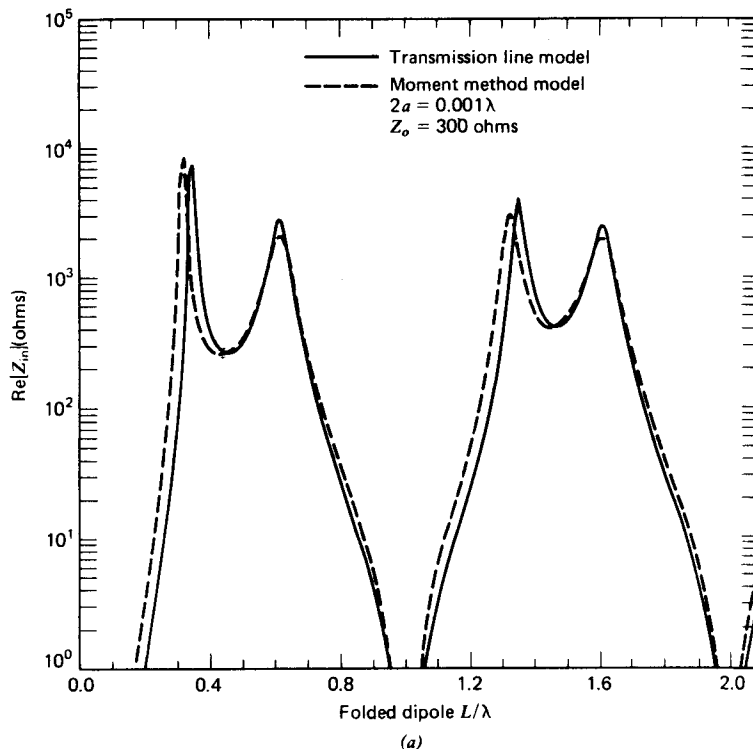


Figure 5-15 Input impedance of a folded dipole. The solid curves are calculated from the transmission line model. The dashed curves are calculated from more accurate numerical methods. The wire radius a is

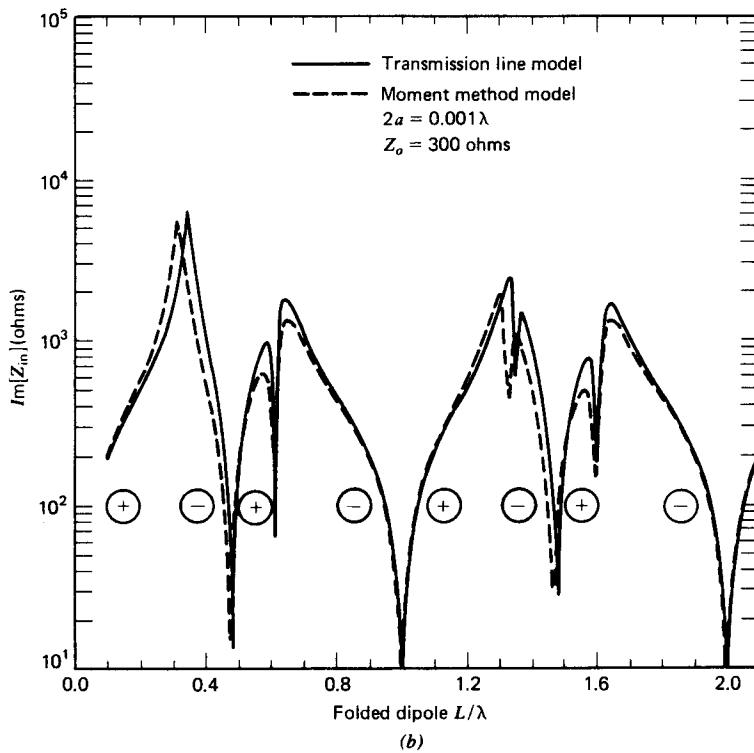
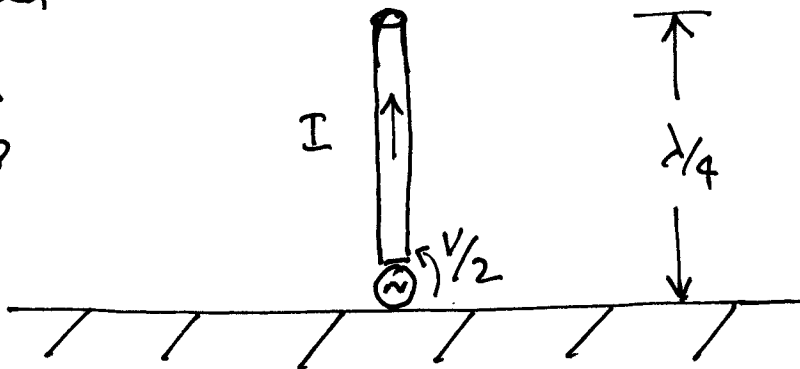


Figure 5-15 (b) Input reactance.

16-38

Above the conducting plane we only need

its field strength changed?
(No!)

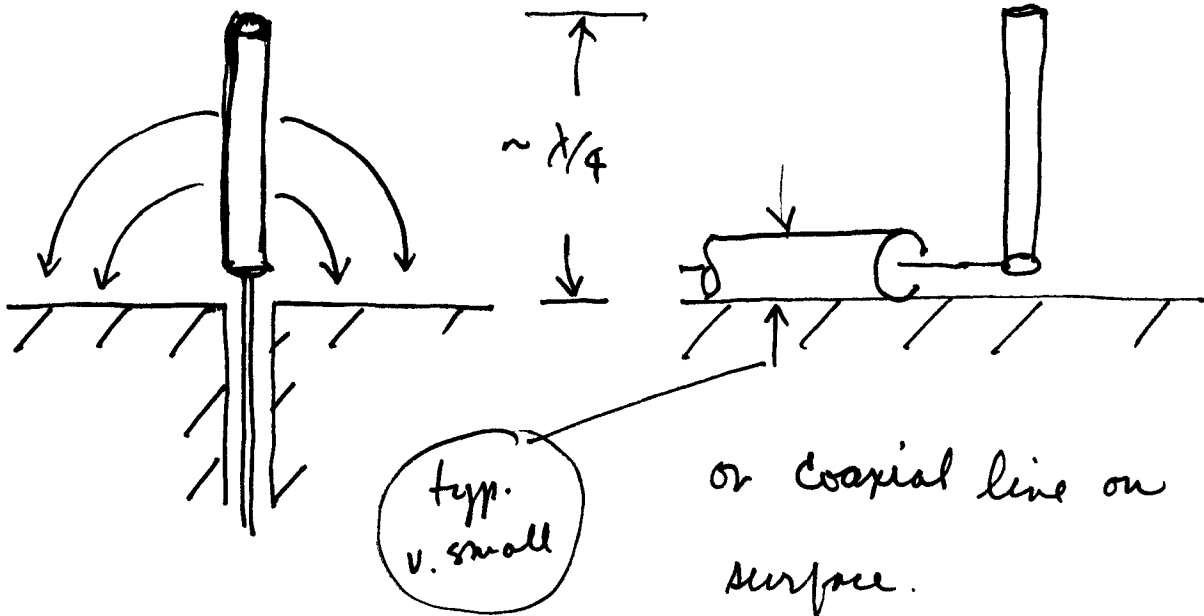


Monopole,
vertical,
"stub"

Has Z_{in} changed? (yes!) $Z_{in} \approx \frac{73}{2} \approx 36 \Omega$

Has input power changed?

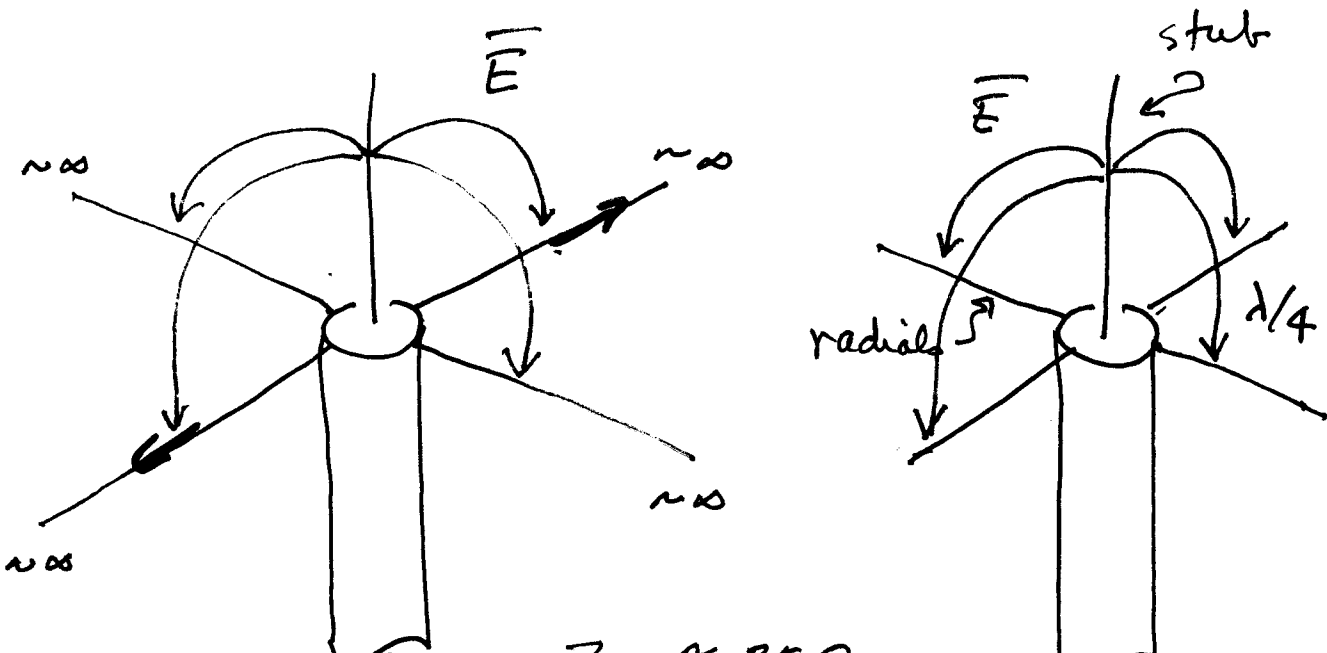
Ways to couple this to a T-Line



Coaxial line
from interior

16-40

As a practical matter, a full ground plane is not required (in many cases)



Other examples of feed structures & monopoles

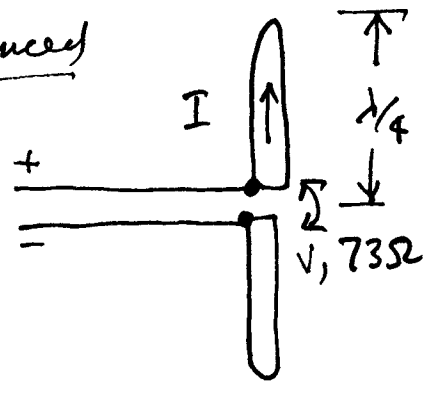
Consider vertical dipole

$$\theta = \frac{\pi}{2}, E_r = 0$$

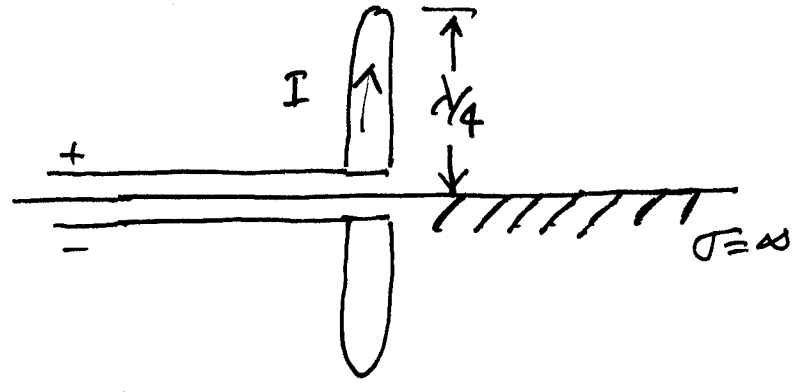
$$E_\theta \neq 0$$

$$H_\phi \neq 0$$

Balanced



in free space



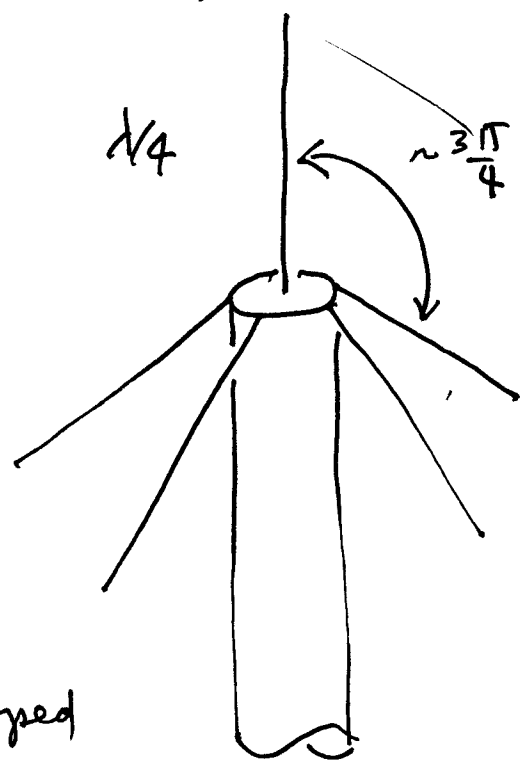
with conducting sheet inserted

are fields different in these two cases.

/...

/... An extremely common antenna looks like this

16-42



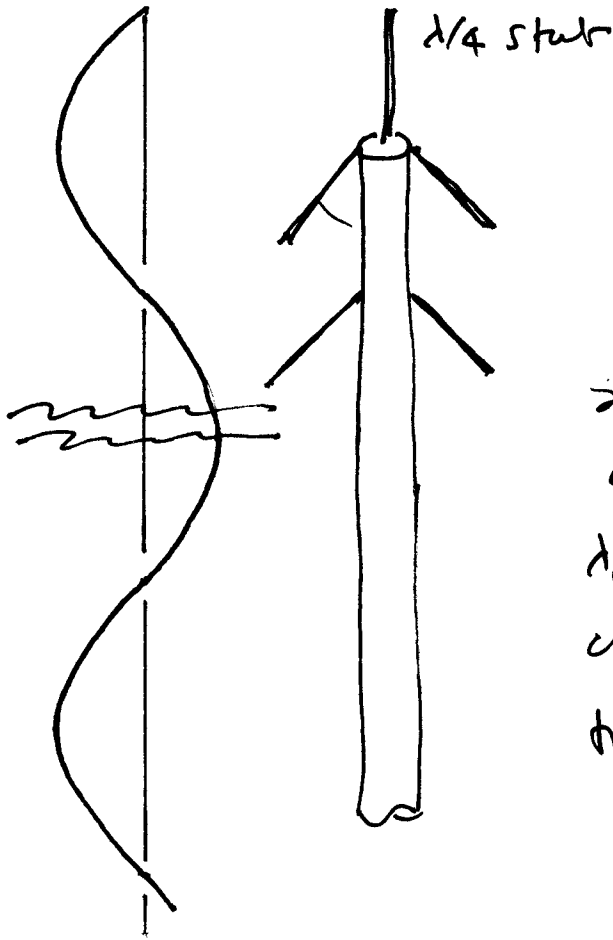
drooped radials

Drooping the radials increases the input Z since the structure (sans transmission line) approaches more closely a $\lambda/2$ dipole. A reasonable match to a 50Ω cable is obtained for

on the transmission line.

Approx.
current
distribution

natural
 I_{max}
about here



Dropped stubs can
function approx. as
 $\lambda/4$ choke - similar
to bazooka balun.

second set of radials
at about this level -
 $\lambda/2$ below feed point -
chokes off current on
transmission line / support
structure.