

**ME111**  
 Instructor: Peter Pinsky  
 Class 8 and 9  
 October 16, 2000

### Today's Topics

- Principal stresses in 3-d.
- Maximum shear stresses in plane stress (re-visited).

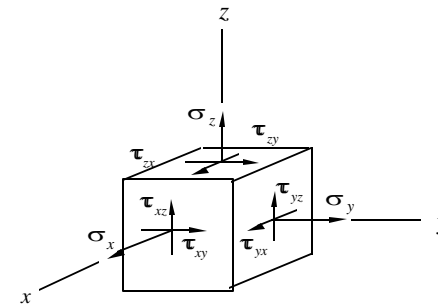
**Reading Assignment** Juvinall 4.8 -- 4.11

October 18, 2000

ME111 Lecture 8/9

1

### 8.1 States of Stress in 3-d



- The stress tensor now has 9 components which can be expressed in components using matrix notation:

$$\boldsymbol{\sigma} \equiv \begin{bmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_y & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_z \end{bmatrix}$$

Only 6 of the components are independent because of symmetry:

$$\tau_{xy} = \tau_{yx}, \quad \tau_{xz} = \tau_{zx}, \quad \tau_{yz} = \tau_{zy}$$

- In 3-d, Mohr's circle is very complicated.

October 18, 2000

ME111 Lecture 8/9

2

## 8.2 Principal Stresses in 3-d

- As designers, we wish to know the largest possible stresses that can exist at a point -- these are called the principal stresses.
- These largest stresses (the principle stresses) will usually determine whether failure of the material will occur or not.
- In most materials we will be more concerned about the magnitude of the principal stresses, and less so with their orientations (one exception - anisotropic materials).

October 18, 2000

ME111 Lecture 8/9

3

## Principal Stresses in 3-d (Continued)

- In 3-d there are 3 principal stress values which are the eigenvalues of the following standard eigenvalue problem:

$$\begin{bmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{xy} & \sigma_y & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & \sigma_z \end{bmatrix} \begin{Bmatrix} n_1 \\ n_2 \\ n_3 \end{Bmatrix} = \sigma \begin{Bmatrix} n_1 \\ n_2 \\ n_3 \end{Bmatrix}$$

For a solution to exist, this requires:

$$\det \begin{bmatrix} \sigma_x - \sigma & \tau_{xy} & \tau_{xz} \\ \tau_{xy} & \sigma_y - \sigma & \tau_{yz} \\ \tau_{xz} & \tau_{yz} & \sigma_z - \sigma \end{bmatrix} = 0$$

- The roots of the determinant polynomial are the principal stresses. The polynomial has the form:

$$\sigma^3 - I_1\sigma^2 + I_2\sigma - I_3 = 0$$

- The quantities  $I_1, I_2, I_3$  are called the stress invariants

$$I_1 = \sigma_x + \sigma_y + \sigma_z$$

$$I_2 = \tau_{xy}^2 + \tau_{yz}^2 + \tau_{zx}^2 - \sigma_x\sigma_y - \sigma_y\sigma_z - \sigma_z\sigma_x$$

$$I_3 = \sigma_x\sigma_y\sigma_z + 2\tau_{xy}\tau_{yz}\tau_{zx} - \sigma_x^2\tau_{yz}^2 - \sigma_y^2\tau_{zx}^2 - \sigma_z^2\tau_{xy}^2$$

October 18, 2000

ME111 Lecture 8/9

4

**Principal Stresses in 3-d (Continued)**

- The principal stresses are ordered so that

$$\sigma_1 \geq \sigma_2 \geq \sigma_3$$

- The planes on which the principal stresses act are mutually orthogonal.
- Once the principal stresses are known, the magnitude of the maximum shear stresses can be determined from:

$$\tau_{13} = \frac{|\sigma_1 - \sigma_3|}{2}$$

$$\tau_{21} = \frac{|\sigma_2 - \sigma_1|}{2}$$

$$\tau_{32} = \frac{|\sigma_3 - \sigma_2|}{2}$$

Maximum occurring shear stress:

$$\tau_{\max} = \max(\tau_{13}, \tau_{21}, \tau_{32})$$

- The maximum shear stresses will occur on planes inclined at  $45^\circ$  to the planes of principal stresses, and will also be mutually orthogonal.

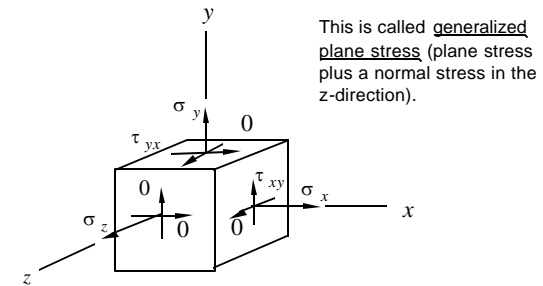
October 18, 2000

ME111 Lecture 8/9

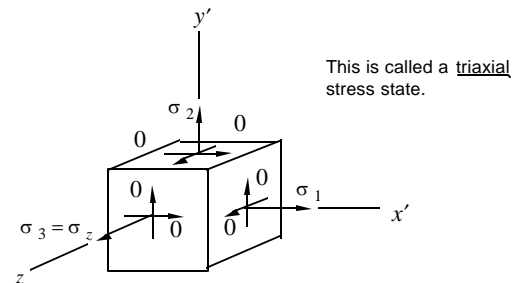
5

**8.3 Triaxial Stress States**

- There is one special case of 3-d stresses that commonly arises that can be easily analyzed.
- Consider the special case where  $\tau_{zx} = \tau_{xz} = 0$



- Transforming the stresses in the x-y plane to principal axes gives:



October 18, 2000

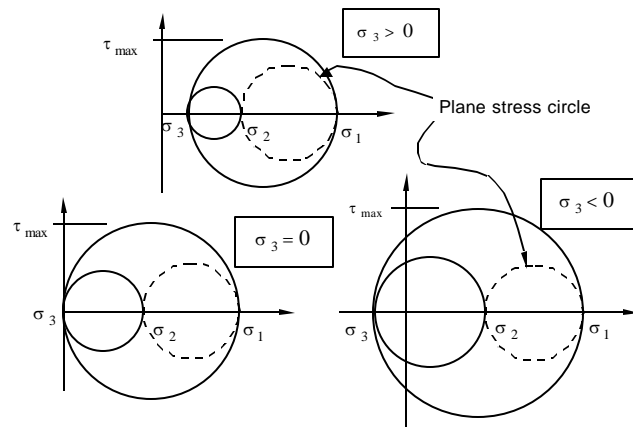
ME111 Lecture 8/9

6

- We know that the maximum shear stresses will occur on planes at  $45^\circ$  to the principal planes.
- The maximum shear stresses are:

$$\begin{aligned}\tau_{13} &= \frac{|\sigma_1 - \sigma_3|}{2} \\ \tau_{21} &= \frac{|\sigma_2 - \sigma_1|}{2} \\ \tau_{32} &= \frac{|\sigma_3 - \sigma_2|}{2}\end{aligned}\quad \tau_{\max} = \max(\tau_{13}, \tau_{21}, \tau_{32})$$

- Graphically, using Mohr's circle, we have (assuming, for example, that  $\sigma_1 > \sigma_2 > 0$  and  $\sigma_1 > \sigma_2 > \sigma_3$ ):



October 18, 2000

ME111 Lecture 8/9

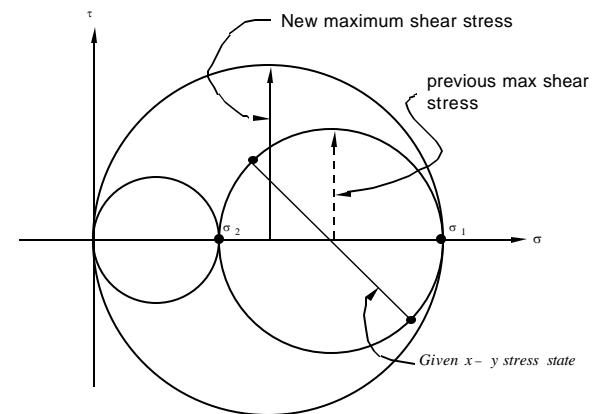
7

#### 8.4 Maximum Shear Stresses in Plane Strain (Re-Visited).

- Once we have the two principal stresses in a plane stress problem, we recognize that the third principal stress (in the z-direction) is zero.
- The maximum shear stress occurring is then:

$$\tau_{\max} = \max(\tau_{13}, \tau_{21}, \tau_{32}) \quad \text{where} \quad \begin{aligned}\tau_{13} &= \frac{|\sigma_1 - 0|}{2} \\ \tau_{21} &= \frac{|\sigma_2 - \sigma_1|}{2} \\ \tau_{32} &= \frac{|0 - \sigma_2|}{2}\end{aligned}$$

Example:



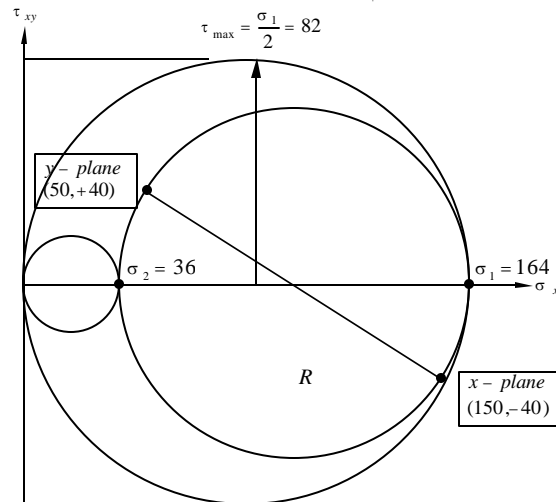
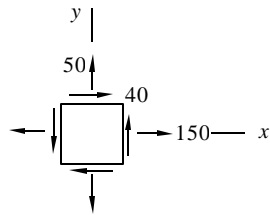
October 18, 2000

ME111 Lecture 8/9

8

**Example 7.4 (Re-Visited)**

Given  $\sigma_x = 150 \text{ MPa}$ ,  
 $\sigma_y = 50 \text{ MPa}$ ,  
 $\tau_{xy} = 40 \text{ MPa}$



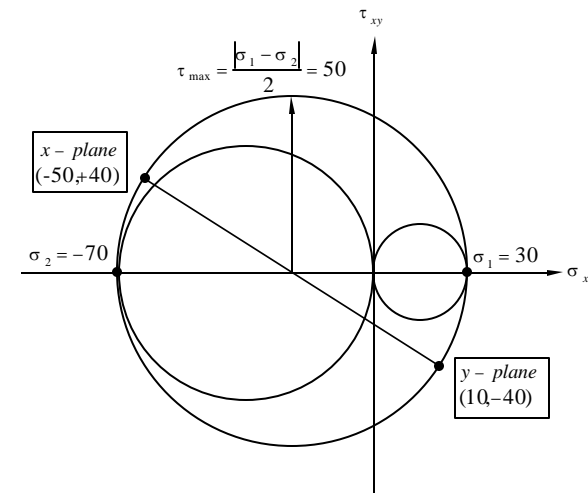
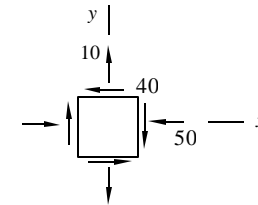
October 18, 2000

ME111 Lecture 8/9

9

**Example 7.5 (Re-Visited)**

Given  $\sigma_x = -50 \text{ MPa}$ ,  
 $\sigma_y = 10 \text{ MPa}$ ,  
 $\tau_{xy} = -40 \text{ MPa}$



October 18, 2000

ME111 Lecture 8/9

10