# **Overhead Slides for**

# Chapter 10

# of

# Fundamentals of Atmospheric Modeling

by

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# Energy Balance for Earth-Atmosphere System





# **Energy Transfer From Equator to Poles**





### **Electromagnetic Spectrum**

Radiation in the form of an electromagnetic wave

Wavelength

$$=\frac{c}{z} = \frac{1}{z} \tag{10.1}$$

#### Radiation in the form of a photon of energy

Energy per unit photon (J photon<sup>-1</sup>)

$$E_p = h = \frac{hc}{(10.3)}$$

Example 10.1.

> > >	Е <sub>р</sub> ~	= 0.5 $\mu$ m = 3.97 x 10 <sup>-19</sup> J photon <sup>-1</sup> = 5.996 x 10 <sup>14</sup> s <sup>-1</sup> = 2 $\mu$ m <sup>-1</sup>
> > >	Е <sub>р</sub> ~	= 10.0 $\mu$ m = 1.98 x 10 <sup>-20</sup> J photon <sup>-1</sup> = 2.998 x 10 <sup>13</sup> s <sup>-1</sup> = 0.1 $\mu$ m <sup>-1</sup>

### **Planck's Law**

Radiance

Intensity of emissions per incremental solid angle

Planck radiance (W m<sup>-2</sup>  $\mu$ m<sup>-1</sup> sr<sup>-1</sup>)

$$B_{,T} = \frac{2hc^2}{5 \exp \frac{hc}{k_B T} - 1}$$
(10.4)

Radiance actually emitted by a substance

$$e = B_{,T} \tag{10.5}$$

Kirchoff's law

In thermodynamic equilibrium, a = --> the efficiency at which a substance absorbs equals that at which it emits.

--> a perfect emitter is a perfect absorber

|--|

Surface Type	Emissivity (fraction)	Surface Type	Emissivity (fraction)	
	(fraction)		(fraction)	
Liquid water	1.0	Soil	0.9 - 0.98	
Fresh snow	0.99	Grass	0.9 - 0.95	
Old snow	0.82	Desert	0.84 - 0.91	
Liq. water clouds	0.25 - 1.0	Forest	0.95 - 0.97	
Cirrus clouds	0.1 - 0.9	Concrete	0.71-0.9	
Ice	0.96	Urban	0.85 - 0.87	

### **Incremental Solid Angle**

Intercepted surface area on a sphere / radius squared d  $a = \frac{dA_s}{r_s^2}$  (10.6)

Incremental surface area  

$$dA_s = (r_s d)(r_s \sin d) = r_s^2 \sin d d$$
 (10.7)

Incremental solid angle (sr) d  $_a = \sin d d$  (10.8)

Solid angle around a sphere

$$a = {a \atop a} d {a = {2 \atop 0 \ 0}} \sin d d = 4$$
 (10.9)

Fig. 10.3. Radiance emitted from point (O) passes through incremental area  $dA_s$  at distance  $r_s$  from the point.



# **Spectral Actinic Flux**

Integral of spectral radiance over all solid angles of a sphere

Incremental spectral actinic flux

$$dE = I \ d \quad a \tag{10.10}$$

Integral of incremental actinic flux over a sphere

$$E = {}_{a} dE = {}_{a} I d {}_{a} = {}_{0}^{2} {}_{0} I \sin d d$$
 (10.11)

Isotropic spectral actinic flux

$$E = I \quad \frac{2}{0 \quad 0} \sin d d = 4 I \quad (10.12)$$

### **Spectral Irradiance**

Flux of radiant energy propagating across a flat surface Incremental spectral irradiance

$$dF = I \cos d_a \tag{10.13}$$

Integral of incremental irradiance over hemisphere of *x*-*y* plane

$$F = dF = I \cos d a = {2 \ 0 \ 0} {I^2 I \cos d d}$$
 (10.14)

Isotropic spectral irradiance

$$F = I \quad \frac{2}{0} \quad \frac{12}{0} \cos \sin d d = I \tag{10.15}$$

Spectral irradiance at the surface of a blackbody

$$F = I = B_{,T}$$
 (10.16)

### **Irradiance**





### Emission Spectra of the Sun and Earth

Fig. 10.5. Irradiance emissions versus wavelength for the sun and earth when both are considered perfect emitters



### <u>Ultraviolet and Visible Portions of</u> <u>Solar Spectrum</u>

Fig. 10.6. Ultraviolet and visible portions of the solar spectrum.



### **Wien's Displacement Law**

Differentiate Planck's law with respect to wavelength at constant temperature and set result to zero

Peak wavelength of emissions from perfect emitter

$$_{p}(\mu m) = \frac{2897}{T(K)}$$
 (10.17)

Example 10.2.		
Sun's photosphere	p = 2897 / 5800  K	= 0.5 µm
Earth's surface	p = 2897 / 288  K	= 10.1 µm

Fig. 10.7. Line through peak irradiances at different temperatures.



# **Stefan-Boltzmann Law**

Integrate Planck irradiance over all wavelength intervals

#### Stefan-Boltzmann law

$$F_b = {}_0 B_{,T} d = {}_B T^4$$
 (10.18)

Stefan-Boltzmann constant

$$B = \frac{2k_B^4}{15h^3c^2} = 5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$$

Example 10.3.

$$T = 5800 \text{ K} ---> F_T = 64 \text{ million W m}^{-2}.$$

$$T = 288 \text{ K} F_T = 390 \text{ W m}^{-2}.$$

# **Reflection and Refraction**

Reflection

Angle of reflection equals angle of incidence

Refraction

Angle of wave propagation relative to a surface normal changes when the density changes





# <u>Albedo</u>

Albedo

#### Fraction of incident sunlight reflected

Table 10.2. Rang	ge of albedos	in the non-UVE	solar spectrum
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Surface Type	Albedo (fraction)	Surface Type	Albedo (fraction)
Earth & atmospher	0.3	Soil	0.05 - 0.2
Liquid water	0.05 - 0.2	Grass	0.16 - 0.26
Fresh snow	0.75 - 0.95	Desert	0.20 - 0.40
Old snow	0.4 - 0.7	Forest	0.10 - 0.25
Thick clouds	0.3 - 0.9	Asphalt	0.05 - 0.2
Thin clouds	0.2 - 0.7	Concrete	0.1 - 0.35
Sea Ice	0.25 - 0.4	Urban	0.1 - 0.27

### **Refraction**

Snell's law

$$\frac{n_2}{n_1} = \frac{\sin 1}{\sin 2}$$
(10.19)

Real part of the index of refraction (1)

Ratio of the speed of light in a vacuum to the speed of light in a given medium

$$n_1 = \frac{c}{c_1}$$
 (10.20)

Real part of the index of refraction of air

$$n_{a}$$
,  $-1 = 10^{-8}$   $8342.13 + \frac{2,406,030}{130 - 2} + \frac{15,997}{38.9 - 2}$  (10.21)

Example 10.4.

	1	= 0.5 µm = 45°
> >	n <sub>air</sub> n <sub>water</sub>	= 1.000279 = 1.335
>	2	= 32°
> >	C <sub>air</sub> C <sub>water</sub>	$= 2.9971 \text{ x } 10^8 \text{ m s}^{-1}$ $= 2.2456 \text{ x } 10^8 \text{ m s}^{-1}$

# **<u>Real Indices of Refraction in Air and</u>** <u>Water Versus Wavelength</u>

Wavelength	Index of	Index of
(µm)	Refraction of Air	Refraction of
		Water
0.2	1.000324	1.396
0.3	1.000292	1.349
0.4	1.000283	1.339
0.5	1.000279	1.335
0.6	1.000277	1.332
0.7	1.000276	1.331
1.0	1.000274	1.327
4.0	1.000273	1.351
7.0	1.000273	1.317
10.0	1.000273	1.218
20.0	1.000273	1.480

#### Table 10.3.

# **Geometry of a Primary Rainbow**

Fig. 10.9.



# **Diffraction Around A Particle**

Huygens' principle

Each point of an advancing wavefront may be considered the source of a new series of secondary waves



# **Radiation Scattering by a Sphere**

Fig. 10.11. Radiation scattering by a sphere.

Ray A is reflected Ray B is refracted twice Ray C is diffracted Ray D is refracted, reflected twice, then refracted Ray E is refracted, reflected once, and refracted

Rays A, B, C, and D scatter in the forward or sideward direction while ray E scatters in the backward direction.



Diffraction

Process by which light bends around objects, and individual wavelengths constructively or destructively interfere with each other

# **Forward and Backscattering**

Fig. 10.12.



Cloud droplets

Scatter primarily in the forward direction

Gas molecules

Scatter evenly in the forward and backward directions

# **Total Internal Reflection**

#### Critical angle

$$2,c = \sin^{-1} \frac{n_1}{n_2} \sin 90^{\circ}$$
(10.22)

#### Example 10.5.

		= 0.5 µm
>	n <sub>air</sub>	= 1.000279
>	<i>n<sub>water</sub></i>	= 1.335
>	2,c	= 48.53°

# <u>Change in Color of the Sun During</u> <u>the Day</u>



Fig. 10.13.

# **Gas Absorption**

	Absorption		Absorption
Gas	Wavelengths (µm)	Gas	Wavelengths (µm)
N <sub>2</sub>	< 0.1	$N_2O_5$	< 0.38
<b>O</b> <sub>2</sub>	< 0.245	HNO <sub>3</sub>	< 0.33
<b>O</b> <sub>3</sub>	0.17 - 0.35, 0.45 - 0.75	$HO_2NO_2$	< 0.33
CO <sub>2</sub>	< 0.21	HCHO	0.25 - 0.36
H <sub>2</sub> O	< 0.21	CH <sub>3</sub> CHO	< 0.345
$H_2O_2$	< 0.35	$CH_3CO_2NO_2$	< 0.3
NO <sub>2</sub>	< 0.71	HC1	< 0.22
N <sub>2</sub> O	< 0.24	CFCL <sub>3</sub>	< 0.23
NO <sub>3</sub>	0.41 - 0.67	$CF_2CL_2$	< 0.23
HONO	< 0.4	CH <sub>3</sub> Cl	< 0.22

Table 10.4. Wavelengths of gas absorption in the solar spectrum.

Fig. 10.15. Extinction coefficient due to NO<sub>2</sub> and O<sub>3</sub> absorption.



# **Infrared Absorption by Gases**

H <sub>2</sub> O	CO <sub>2</sub>	O <sub>3</sub>	N <sub>2</sub> O	CH <sub>4</sub>	$CF_2Cl_2$	CFCl <sub>3</sub>	CH <sub>3</sub> Cl
0.72	1.4	9.6	4.5	3.31	8.6	11.8	11.8
0.82	1.6	14.27	7.78	3.43	9.13	9.2	
0.94	2.0		17.0	6.55			
1.1	2.7			7.65			
1.38	4.3						
1.87	4.8						
2.7	5.2						
3.2	15.0						
6.25							
> 12.0							

Table 10.5. Peak absorption wavelength bands ( $\mu$ m) of several greenhouse gases. Data from (Liou, 1992)

Efficiency of absorption compared to CO<sub>2</sub> (IPCC, 1990)

$CH_4$	= 21  x more efficient
N <sub>2</sub> O	= 206  x more efficient

 $N_2O$  = 206 x more efficient CFCl<sub>3</sub> = 12,400 times more efficient

# **Extinction Coefficient**

Fig. 10.14. Attenuation of incident radiance,  $I_0$ , due to absorption as it travels through a column of gas.



Extinction coefficient ( ) (cm<sup>-1</sup>, m<sup>-1</sup>, or km<sup>-1</sup>) A measure of the loss of radiation per unit distance

Example

Reduction in radiance with distance through a gas

$$\frac{dI}{dx} = -N_q b_{a,g,q}, \ TI = -a_{,g,q}, \ TI$$
(10.23)

Integrate

$$I = I_0, \ e^{-N_q b_{a,g,q,,T}(x-x_0)} = I_0, \ e^{-a,g,q,,T(x-x_0)}$$
(10.24)

# **Extinction Coefficient**

Extinction coefficient due gas absorption

$$a,g, = N_{ag} N_{q} b_{a,g,q}, \quad T = a,g,q, \quad T$$
(10.25)  
$$a,g, q = 1 q = 1$$

Meteorological range (Koschmieder equation)

$$x = \frac{3.912}{ext,}$$

Table 10.6. Extinction coefficients () and meteorological ranges (x) due to NO<sub>2</sub> absorption and meteorological range due to Rayleigh scattering ( $x_{sg}$ , ).

		NO <sub>2</sub> (ppmv)				
		<0.01>		<0.25>		
	b	<i>a.g</i>	$x_{a,g}$	<i>a.g</i>	$x_{a,g}$	$x_{s,g}$
μm	$10^{-19} \mathrm{cm}^2$	$10^8 \mathrm{cm}^{-1}$	km	$10^{-8} \text{ cm}^{-1}$	km	km
0.42	5.39	13.2	296	330	11.8	112
0.45	4.65	11.4	343	285	13.7	148
0.50	2.48	6.10	641	153	25.6	227
0.55	0.999	2.46	1590	61.5	63.6	334
0.60	0.292	0.72	5430	18.0	217	481
0.65	0.121	0.30	13,000	7.5	520	664

# **Gas Scattering**

Rayleigh scatterer: 2 r/ <<1

Extinction coefficient due to Rayleigh scattering

$$s,g, = N_a b_{s,g},$$
 (10.27)

Scattering cross section of a typical air molecule (cm<sup>2</sup>)

$$b_{s,g,} = \frac{8 \left[\frac{3\left(n_{a,}^{2} - 1\right)^{2}}{3 \left[\frac{4}{N_{a,0}^{2}}\right]^{2}} f(*) - \frac{32 \left[\frac{3\left(n_{a,} - 1\right)^{2}}{3 \left[\frac{4}{N_{a,0}^{2}}\right]^{2}} f(*) - (10.28)\right]}{3 \left[\frac{4}{N_{a,0}^{2}}\right]^{2}}$$

Anisotropic correction factor

$$f(*) = \frac{6+3}{6-7} \frac{*}{*} \quad 1.05 \tag{10.29}$$

# **Rayleigh Scattering Example**

Example 10.6.

		= 0.5 µm
	р	= 1 atm (sea level)
	Т	= 288 K
>	<i>s</i> , <i>g</i> ,	$= 1.72 \text{ x } 10^{-7} \text{ cm}^{-1}$
>	x	= 227 km

$$= 55 \ \mu m$$
  
--->  $s,g, = 1.17 \ x \ 10^{-7} \ cm^{-1}$   
--->  $x = 334 \ km$ 

# **Imaginary Index of Refraction**

Determines extent to which a substance absorbs radiation

Fig. 10.16. Attenuation of incident radiance,  $I_0$ , due to absorption as it travels through a particle.



Attenuation of radiation due to particle absorption

$$\frac{\mathrm{d}I}{\mathrm{d}x} = -\frac{4}{I} \tag{10.30}$$

Integrate

$$I = I_0 e^{-4} (x - x_0) /$$
(10.31)

# **Complex Index of Refraction**

m = n - i.

(10.32)

Table 10.7. Real and imaginary indices of refraction for some substances at = 0.50 and  $10.0 \ \mu m$ .

	0.5 µm		10 µm		
	Real $(n)$	Imaginary ( )	Real $(n)$	Imaginary ( )	
H <sub>2</sub> O (aq)	1.34	1.0 x 10 <sup>-9</sup>	1.22	5.0 x 10 <sup>-2</sup>	
Elemental C (s)	1.82	7.4 x 10 <sup>-1</sup>	2.40	1.0 x 10 <sup>0</sup>	
Organic C (s)	1.45	1.0 x 10 <sup>-3</sup>	1.77	1.2 x 10 <sup>-1</sup>	
$H_2SO_4$ (aq)	1.43	1.0 x 10 <sup>-8</sup>	1.89	4.6 x 10 <sup>-1</sup>	
$(NH_4)_2SO_4(s)$	1.52	5.0 x 10 <sup>-4</sup>	2.15	2.0 x 10 <sup>-2</sup>	
NaCl(s)	1.45	1.5 x 10 <sup>-4</sup>	1.53	5.3 x 10 <sup>-2</sup>	

Table 10.8. Light transmission through particles at  $= 0.50 \ \mu m$ .

Substance and	Particle Diameter	Transmission ( $I   I_0$ )
	(µm)	
Elemental carbon $(=0.74)$	0.1	0.16
	1.0	8.0 x 10 <sup>-9</sup>
	10.0	0
Water ( $=10^{-9}$ )	0.1	0.999999997
	1.0	0.99999997
	10.0	0.9999997

# Imaginary Index of Refraction of Liquid Nitrobenzene

Fig. 10.17



# **<u>Particle Extinction Coefficients</u>**

Particle absorption and scattering extinction coefficients

$$a,a, = N_B i = 1$$
(10.33)  
$$s,a, = N_B i = 1 (10.33)$$
  
$$i = 1$$
(10.33)

Absorption and scattering cross sections of a particle (cm<sup>2</sup>)

$$b_{a,a\,i,} = r_i^2 Q_{a,i,} \tag{10.34}$$

$$b_{s,a\,i} = r_i^2 Q_{s,i} \tag{10.34}$$

Size parameter

$$i_{i} = 2 r_{i} / (10.35)$$

# **Tyndall Absorption / Scattering**

Rayleigh regime 
$$(r_i << 0.1 \text{ or } i, < 0.1)$$

Single particle Tyndall absorption efficiency  $r_i$ /

$$Q_{a,i,} = -4\frac{2 r_i}{m^2 + 2} \operatorname{Im} \left| \frac{m^2 - 1}{m^2 + 2} \right|^2 = \frac{2 r_i}{(n^2 + 2)^2 + 4(n^2 - 2 + 1)}$$
(10.36)

$$0 \to Q_{a,i}$$
,  $= \frac{2 r_i}{\left(n^2 + 2\right)^2} \xrightarrow{--> \text{linear with}} (10.37)$ 

Single particle Tyndall scattering efficiency  $(r_i / )^4$ 

$$Q_{s,i} = \frac{8}{3} \frac{2 r_i}{m^2 + 2} \left| \frac{m^2 - 1}{m^2 + 2} \right|^2$$
(10.38)

Example 10.7. (liquid water)  

$$= 0.5 \ \mu m$$
  $r_i = 0.01 \ \mu m$   
 $---> n = 1.34 ---> = 1.0 \ x \ 10^{-9}$   
 $---> Q_{s,i} = 2.92 \ x \ 10^{-5}$   
 $---> Q_{a,i} = 2.8 \ x \ 10^{-10}$ 

# **Mie Absorption / Scattering**

Mie regime (
$$r_i \sim 0.1 < i_i < 100$$
)

Single particle Mie scattering efficiency

$$Q_{s,i,} = \frac{2}{i} (2k+1) \left( \left| a_k \right|^2 + \left| b_k \right|^2 \right)$$
(10.39)

Single particle Mie absorption efficiency

$$Q_{a,i}$$
, =  $Q_{e,i}$ , -  $Q_{s,i}$ ,

Single particle total extinction coefficient

$$Q_{e,i,} = \frac{2}{i, k=1} (2k+1) \operatorname{Re}(a_k + b_k)$$
 (10.40)

### <u>Single Particle Absorption / Scattering</u> <u>Efficiency by Soot</u>

Fig. 10.18.  $Q_a$ ,  $Q_s$ , and  $Q_f$  of elemental carbon (soot) particles at = 0.50 µm (n = 1.94, = 0.66). The efficiency for soot at any other visible wavelength  $_1$  and diameter  $d_1$  is the efficiency at diameter, d = 0.5µm ×  $d_1/_1$ .



### <u>Single Particle Absorption / Scattering</u> <u>Efficiency by Water</u>

Fig. 10.19.  $Q_a$ ,  $Q_s$ , and  $Q_f$  of liquid water drops of different sizes at a wavelength of  $= 0.50 \ \mu m \ (n = 1.34, = 0.)$ . The efficiency for water at any other visible wavelength  $_1$  and diameter  $d_1$  is the efficiency at diameter,  $d = 0.5 \ \mu m \times d_1 / _1$ .



# **Geometrical Scattering / Absorption**

Geometrical regime  $(i, > 100) \rightarrow significant diffraction$ In the limit (i, j), scattering efficiency is constant  $\lim_{i} Q_{s,i} = 1 + \left| \frac{m - 1}{m + 2} \right|$ (10.41)i, Example 10.8.  $= 0.5 \ \mu m$ n = 1.34 for liquid water --->  $Q_{s,i}$ , = 1.1 as *i*, from (10.41) --->  $Q_{a,i}$ , = 1.1 as *i*, from fig (10.18) regardless of how weak the Also, as  $Q_{s,i}$  $Q_{a,i}$ i, , imaginary index of refraction is.

#### Volume-averaged effective index of refraction

$$n = \frac{N_V}{q=1} \frac{v_{q,i}}{v_i} n , q$$
(10.42)

### **Predicted Extinction Coeff. Profiles**



Fig. 10.20 b.

# **Visibility Definitions**

#### Meteorological range

Distance from an ideal dark object at which the object has a 0.02 liminal contrast ratio against a white background

#### Liminal contrast ratio

Lowest visually perceptible brightness contrast a person can see

#### Visual range

Actual distance at which a person can discern an ideal dark object against the horizon sky

#### Prevailing visibility

Greatest visual range a person can see around a 180° horizontal arc, but nut necessarily in continuous sectors around the arc

Fig. 10.21. At point x, the intensity of the radiation originating from the direction of an object has increased to the background intensity.



# **Meteorological Range**

Change in object intensity along path of radiation

$$\frac{dI}{dx} = bI_B - extI$$
(10.43)  

$$I_B = \text{constant background intensity (radiance) of light,}$$

$$bI_B = \text{constant scattering of background light back into the line of vision along the path}$$

$$ext = \text{extinction coefficient due to absorption and scattering along the path}$$

Change in background intensity

$$\frac{\mathrm{d}I_B}{\mathrm{d}x} = bI_B - extI_B = 0 \tag{10.44}$$

Substitute b = ext into (10.43)

$$\frac{\mathrm{d}I}{I_B - I} = ext \,\mathrm{d}x. \tag{10.45}$$

Integrate from  $I_0 = 0$  to I and  $x_0 = 0$  to x

$$C_{ratio} = \frac{I_B - I}{I_B} = e^{-ext^X}$$
 (10.46)

Meteorological range (Koschmieder equation)

$$x = \frac{3.912}{ext}$$
(10.47)

# **Meteorological Range**

Table 10.9. Meteorological ranges due to scattering by gases (*sg*), absorption by gases (*ag*), scattering by particles (*sp*), absorption by particles (*ap*), and total extinction (*ext*) at  $= 0.55 \ \mu m$  in Los Angeles. (Larson, 1984).

	Meteorological Range (km)				
	$x_{Sg}$ ,	$x_{ag}$ ,	$x_{sp}$ ,	$x_{ap}$ ,	$x_{ext}$ ,
Clean day (4 / 7 / 83)	352	326	151	421	67.1
Polluted day (8 / 25 / 83)	366	130	9.59	49.7	7.42

### **Optical Depth**

Total extinction coefficient

$$= s, g, + a, g, + s, a, + a, a, + s, c, + a, c,$$
(10.48)

Incremental distance vs. incremental path length

$$dz = \cos_{s} dS_{b} = \mu_{s} dS_{b} \tag{10.49}$$

Incremental optical depth

$$\mathbf{d} = - \mathbf{d}z = - \boldsymbol{\mu}_s \mathbf{d}S_b \tag{10.51}$$

Optical depth as a function of altitude

$$= {}^{z} dz = {}^{S_{b}} \mu_{s} dS_{b}$$
(10.52)

Fig. 10.22. Relationship between optical depth, altitude, solar zenith angle, and pathlength.



# Solar Zenith Angle

Cosine of solar zenith angle

```
\cos_s = \sin \sin + \cos \cos \cos H_a \tag{10.53}
```

Solar declination angle ( )

Angle between the equator and the north or south latitude of the subsolar point

Subsolar point

Point at which the sun is directly overhead

Local hour angle ( $H_a$ )

Angle, measured westward, between longitude of subsolar point and longitude of location of interest.

Figs. 10.23 b. Geometry for zenith angle calculations.



### **Solar Declination Angle**

Solar declination angle

$$=\sin^{-1}\left(\sin_{ob}\sin_{ec}\right) \tag{10.54}$$

Obliquity of the ecliptic

Angle between the plane of the earth's equator and the plane of the ecliptic, which is the mean plane of the earth's orbit around the sun.

$$ob = 23^{\circ}.439 - 0^{\circ}.0000004 N_{JD}$$
(10.55)

Ecliptic longitude of earth

$$e_{c} = L_{M} + 1^{\circ}.915 \sin g_{M} + 0^{\circ}.020 \sin 2g_{M}$$
 (10.57)

Mean longitude of the sun

$$L_M = 280^{\circ}.460 + 0^{\circ}.9856474 N_{JD} \tag{10.58}$$

Mean anomaly of the sun

$$g_M = 357^\circ.528 + 0^\circ.9856003N_{JD} \tag{10.58}$$

### **Solar Zenith Angle**

Local hour angle

$$H_a = \frac{2 t_s}{86,400} \tag{10.59}$$

#### Example.

At noon, when sun is directly overhead,  $H_a = 0 --->$ 

 $\cos s = \sin sin + \cos cos$ 

When the sun is over the equator, the = 0 --->

 $\cos_s = \cos \cos H_a$ 

#### Example 10.9.

	1:00 p.n	n., PST, Feb. 27, 1994, $= 35 $ °N.
>	$D_J$	= 58
>	N <sub>JD</sub>	= -2134.5
>	<i>8m</i>	= -1746.23°
>	$L_m$	$= -1823.40^{\circ}$
>	се	$= -1821.87^{\circ}$
>	ob	= 23.4399°
>		= -8.52°
>	$H_a$	$= 15.0^{\circ}$
>cos	$s = \sin($	$35^{\circ}$ sin $(-8.52^{\circ})$ + cos $(35^{\circ})$ cos $(-8.52^{\circ})$ cos $(15.0^{\circ})$
>	S	$=45.8^{\circ}$

### **Solstices and Equinoxes**

Fig. 10.24. Solar declinations during solstices and equinoxes. The earth-sun distance is greatest at the summer solstice.



### **Radiative Transfer Equation**

Change in radiance / irradiance along a beam of interest

Change in radiance along incremental path length

 $dI = -dI_{so}, -dI_{ao}, +dI_{si}, +dI_{si}, +dI_{ei},$ (10.60)

Scattering of radiation out of the beam

$$\mathrm{d}I_{SO,} = I \quad s, \ \mathrm{d}S_b \tag{10.61}$$

Absorption of radiation along the beam

 $dI_{ao} = I_{a} dS_b$ (10.62)

Multiple scattering of diffuse radiation into the beam

Single scattering of direct solar radiation into the beam

$$dI_{Si,} = \frac{s,k}{4} P_{s,k,\mu,-\mu_s,\sigma,\sigma} F_{s,\sigma} e^{-I\mu_s} dS_b$$
(10.64)

Emissions of infrared Planckian radiation into the beam

$$dI_{ei} = a, B_{T} dS_b \tag{10.65}$$

# **Extinction Coefficients**

Extinction due to total scattering only

$$s_{s,} = s_{s,g} + s_{s,a} + s_{s,c},$$
 (10.66)

Extinction due to total absorption only

$$a_{1} = a_{1}g_{1} + a_{2}a_{1} + a_{3}c_{1}$$
 (10.66)

Total extinction due to scattering plus absorption

$$= s, + a,$$
 (10.67)

## **Scattering Phase Function**

Gives angular distribution of scattered energy vs. direction

Scattering phase function for diffuse radiation

 $P_{s,k}$ ,  $\mu,\mu$ , redirects diffuse radiation from  $\mu$ , to  $\mu$ ,

Scattering phase function for direct radiation

 $P_{s,k}$ ,  $\mu,-\mu_s$ ,  $\mu_s$  redirects direct solar radiation from  $-\mu$ , s to  $\mu$ ,

Fig. 10.25. Single scattering of direct solar radiation and multiple scattering of diffuse radiation.



### **Scattering Phase Function**

Scattering phase function defined such that

$$\frac{1}{4} \quad _{4} \quad P_{s,k}$$
, ()d  $_{a} = 1$  (10.68)

 $= angle \ between \ directions \ \mu \ , \qquad and \ \mu \ ,$ 

Substitute d  $a = \sin d d \rightarrow a$ 

$$\frac{1}{4} \begin{array}{c} 2\\ 0 \\ 0 \end{array} P_{s,k}, \quad () \sin d d = 1 \quad (10.69)$$

Phase function for isotropic scattering

$$P_{S,k}$$
, () = 1 (10.70)

Phase function for Rayleigh scattering

$$P_{s,k}$$
, () =  $\frac{3}{4} \left( 1 + \cos^2 \right)$  (10.71)

### **Scattering Phase Functions**

Figs. 10.26 a and b. Scattering phase functions for (a) isotropic and (b) Rayleigh scattering.





**(b)** 

# **Asymmetry Factor**

First moment of phase function -- gives relative direction of scattering by particles or gases

In general,

$$\begin{array}{ll} > 0 & \text{forward (Mie) scattering} \\ g_{a,k,} &= 0 & \text{isotropic or Rayleigh scattering} \\ < 0 & \text{backward scattering} \end{array}$$
 (10.73)

$$g_{a,k,} = \frac{1}{4} P_{s,k,}$$
 ()cos d a (10.72)

Expand with d  $a = \sin d d \rightarrow a$ 

$$g_{a,k,} = \frac{1}{4} \begin{bmatrix} 2 \\ 0 & 0 \end{bmatrix} P_{s,k,}$$
 () cos sin d d (10.74)

Isotropic Scattering  $---> P_{s,k}$ , () =1 --->

$$g_{a,k}$$
,  $=\frac{1}{4} \begin{bmatrix} 2 \\ 0 \end{bmatrix} \cos \sin d d = -\frac{1}{2} \begin{bmatrix} -1 \\ \mu d\mu \end{bmatrix} = 0$  (10.75)

Rayleigh scattering --->

$$g_{a,k,} = \frac{1}{4} \frac{2}{0} \frac{3}{4} \left(1 + \cos^2\right) \cos \sin d d$$
$$= -\frac{3}{8} \frac{2}{0} \frac{-1}{1} \left(\mu + \mu^3\right) d\mu d = 0$$
(10.76)

Mie scattering --->

$$g_{a,k} = Q_{f,i} / Q_{s,i},$$
 (10.78)

# **Incident Solar Flux**

Cumulative irradiance (W m<sup>-2</sup>) emitted by sun's photosphere

$$F_p = \frac{L_p}{4 R_p^2} = B T_p^4$$
(10.79)

 $L_p$  = emissions from sun's photosphere = 3.9 x 10<sup>26</sup> W

$$R_p$$
 = radius from sun center to photosphere = 6.96 x 10<sup>8</sup> m

$$T_p$$
 = temperature of photosphere =  $T_p$  = 5796 K

#### Example 10.10. $T_p = 5796 \text{ K}$ $--> F_p = 6.4 \times 10^7 \text{ W m}^{-2}$

### **Solar Constant**

Mean cumulative irradiance at top of earth's atmosphere

$$\overline{F}_{s} = \frac{R_{p}}{\overline{R}_{es}}^{2} F_{p} = \frac{R_{p}}{\overline{R}_{es}}^{2} BT_{p}^{4}$$
(10.80)  
Calculated  $\overline{F}_{s}$  1379 W m<sup>-2</sup>  
Observed  $\overline{F}_{s}$  1365 W m<sup>-2</sup>

Varies by +/- 1 W m<sup>-2</sup> over each 11 year sunspot cycle

Daily cumulative irradiance depends on earth-sun distance

$$F_{s} = \frac{R_{es}}{\overline{R}_{es}}^{2} \overline{F}_{s}$$
(10.81)

#### Empirical formula

$$\frac{R_{es}}{\overline{R}_{es}} \stackrel{2}{=} 1.00011 + 0.034221 \cos \ J + 0.00128 \sin \ J \\ + 0.000719 \cos 2 \ J + 0.000077 \sin 2 \ J$$
(10.82)

$$J = 2 D_J / D_Y$$
(10.83)

## **Incident Solar Flux**

Example 10.11.

December 22 --->  $F_s$  = 1365 x 1.034 = 1411 W m<sup>-2</sup>

June 22 --->  $F_s$  = 1365 x 0.967 = 1321 W m<sup>-2</sup>

Irradiance varies by 90 W m<sup>-2</sup> (6.6%) between Dec. and June.

Cumulative solar irradiance as sum of spectral irradiances

$$F_{s} = \left(F_{s}, \right) = \frac{R_{es}}{\overline{R}_{es}}^{2} \left(\overline{F}_{s}, \right) = \frac{R_{es}}{\overline{R}_{es}}^{2} \overline{F}_{s} \quad (10.83)$$

### **Seasons**

Fig. 10.27. Relationship between the sun and earth during the solstices and equinoxes.



### **Equilibrium Earth Temperature**

Energy (W) absorbed by the earth-atmosphere system

$$E_{\rm in} = \overline{F}_s \left( 1 - A_{e,0} \right) \left( \begin{array}{c} R_e^2 \right) \tag{10.84}$$

Energy emitted by the earth's surface

$$E_{\text{out}} = e_{,0} \quad BT_e^4 \left( 4 \ R_e^2 \right) \tag{10.85}$$

Equate --> temperature without greenhouse effect

$$T_e = \frac{\overline{F}_s \left(1 - A_{e,0}\right)}{4} \frac{1/4}{e, 0}$$
(10.86)

Example 10.12.

$$\overline{F}_{s} = 1365 \text{ W m}^{-2} \\
A_{e,0} = 0.3 \\
---> T_{e} = 254.8 \text{ K}$$

Actual average surface temperature on earth 288 K --> difference due to absorption by greenhouse gases

# **Radiative Transfer Equation**

$$s, = \frac{s}{s} = \frac{s, g, + s, a, + s, c,}{s, g, + a, g, + s, a, + a, a, + s, c, + a, c,}$$

Total extinction coefficient

$$=$$
 s,  $+$  a,

Optical depth

$$d = - \mu_s dS_b$$

# **Radiative Transfer Equation**

#### Rewrite radiative transfer equation

$$\mu \frac{dI_{,\mu,}}{d} = I_{,\mu,} - J_{,\mu,}^{diffuse} - J_{,\mu,}^{direct} - J_{,\mu,}^{emis}$$
(10.89)

where

$$J_{\mu,\mu}^{diffuse} = \frac{1}{4} \int_{k}^{k} \frac{s_{,k,\mu}}{0} \frac{2}{-1} I_{\mu,\mu}, P_{s,k,\mu,\mu,\mu,\mu}, d\mu d$$
(10.90)

$$J_{\mu,\mu}^{direct} = \frac{1}{4} F_{s,\mu} e^{-I\mu_{s}} \frac{s,k}{k} P_{s,k,\mu,\mu,\mu_{s},\mu_{s},\mu_{s}}$$
(10.91)

 $J_{\mu,\mu}^{emis} = \begin{pmatrix} 1 - s \end{pmatrix} B_{\mu,T}.$  (10.92)

### **Beer's Law**

Consider only absorption in downward direction

$$-\mu \frac{dI_{,-\mu,}}{d_{a,}} = I_{,-\mu,}$$
(10.93)

Solution

$$I_{,-\mu,} (a,) = I_{,-\mu,} (a, t) e^{-(a, -a, t)/\mu}$$
(10.95)

# **Schwartzchild's Equation**

Consider absorption and infrared emissions

$$-\mu \frac{dI_{,-\mu,}}{d_{a,}} = I_{,-\mu,} - B_{,T}$$
(10.96)

Solution

$$I_{,-\mu}, (a, ) = I_{,-\mu}, (a, t)e^{-(a, -a, t)/\mu}$$
$$+ \frac{1}{\mu} a_{,,t}^{a, B}, T(a, )e^{-(a, -a, t)/\mu} d_{a,}$$
(10.98)

### **Two-Stream Method**

Divide phase function into upward (+) and downward component

#### Integrated fraction of forward scattered energy

$$1 - b = \frac{1 + g_{a,}}{2} \tag{10.101}$$

#### Integrated fraction of backscattered energy

$$b = \frac{1 - g_a}{2} \tag{10.101}$$

#### Effective asymmetry parameter

$$g_{a,} = \frac{s,a, g_{a,a,} + s,c, g_{a,c,}}{s,g, + s,a, + s,c,}$$
(10.102)

# **Predicted Asymmetry Parameter and Single-Scattering Albedo**

Fig. 10.28 a



# **<u>Predicted Asymmetry Parameter and</u>** <u>Single-Scattering Albedo</u>

Fig. 10.28 b



### **Two-Stream Approximation**

Upward radiance equation

$$\mu_1 \frac{dI_+}{d} = I_+ - s(1-b)I_+ - sbI_- - \frac{s}{4}(1 - 3g_a\mu_1\mu_s)F_se^{-I\mu_s}$$

Downward radiance equation

$$-\mu_1 \frac{dI_-}{d} = I_- - s(1-b)I_- - sbI_+ - \frac{s}{4}(1+3g_a\mu_1\mu_s)F_se^{-I\mu_s}$$

Upward and downward irradiances in terms of radiance for twostream approximation

$$F_{+} = 2 \ \mu_{1}I_{+}$$
  $F_{-} = 2 \ \mu_{1}I_{-}$ 

Substitute irradiances and generalize for different approximations to phase function

Solar irradiance

$$\frac{\mathrm{d}F_{+}}{\mathrm{d}} = {}_{1}F_{+} - {}_{2}F_{-} - {}_{3} {}_{s}F_{s}e^{-} /\mu_{s}$$
(10.106)

$$\frac{\mathrm{d}F_{-}}{\mathrm{d}} = - \,_{1}F_{-} + \,_{2}F_{+} + \left(1 - \,_{3}\right) \,_{s}F_{s}e^{-/\mu_{s}} \tag{10.106}$$

Surface boundary condition

 $F_{+,N_L+1/2} = A_e F_{-,N_L+1/2} + \frac{A_e \mu_s F_s e^{-N_L+1/2}}{B_T} \frac{1}{12} + \frac{1}{12} \frac{$ 

(10.104)

(10.105)

(10.108)

# **Two-Stream Approximation**

Table 10.10. Coefficients for two stream approximations using two techniques.

Approximation	1	2	3
Quadrature	$\frac{1 - \frac{s(1+g_a)}{2}}{\mu_1}$	$\frac{s(1-g_a)}{2\mu_1}$	$\frac{1-3g_a\mu_1\mu_s}{2}$
Eddington	$\frac{7 - s(4 + 3g_a)}{4}$	$-\frac{1-s(4-3g_a)}{4}$	$\frac{2-3g_a\mu_s}{4}$

Infrared irradiance

$$\frac{\mathrm{d}F_{+}}{\mathrm{d}} = {}_{1}F_{+} - {}_{2}F_{-} - 2 \left(1 - {}_{s}\right)B_{T}$$
(10.107)

$$\frac{\mathrm{d}F_{-}}{\mathrm{d}} = - \,_{1}F_{-} + \,_{2}F_{+} + 2 \, \left(1 - \,_{s}\right)B_{T} \tag{10.107}$$

### **Delta Functions**

Quadrature and Eddington solutions underpredict forward scattering because expansion of phase function is too simple to obtain the strong peak in scattering efficiency.

--> adjust terms with delta functions

$$g_{a} = \frac{g_{a}}{1 + g_{a}}$$
(10.109)  

$$s = \frac{\left(1 - g_{a}^{2}\right) s}{1 - s g_{a}^{2}}$$
(10.109)  

$$= \left(1 - s g_{a}^{2}\right)$$
(10.109)

# **Heating Rates**

Net flux divergence equation

$$\frac{T}{t} = \frac{1}{c_{p,m}} \frac{\mathrm{d}Q_{solar}}{\mathrm{d}t} + \frac{\mathrm{d}Q_{ir}}{\mathrm{d}t} = \frac{1}{c_{p,m}} \frac{F_n}{z}$$
(10.110)

Net downward minus upward radiative flux

$$F_n = \int_0 \left(F_{-,} - F_{+,}\right) d$$

Partial derivative term

$$\frac{F_{n,k}}{z} \qquad \frac{\left[\left(F_{-, k-1/2} - F_{+, k-1/2}\right) - \left(F_{-, k+1/2} - F_{+, k+1/2}\right)\right]}{z_{k-1/2} - z_{k+1/2}}$$

(10.111)

Temperature change

$$T_k = \frac{1}{c_{p,m-a}} \frac{F_n}{z} h$$
 (10.112)

### **Photolysis Coefficients**

Photolysis rate (s<sup>-1</sup>) at bottom of layer k

$$J_{q, p, k+1/2} = {}_{0}4 I_{p, k+1/2}b_{a, g, q, T}Y_{q, p, T}d$$
(10.113)

Radiance at bottom of layer k (photons cm<sup>-2</sup>  $\mu$ m sr<sup>-1</sup> s<sup>-1</sup>)

$$I_{p, k+y_2} = \left(I_{-, k+y_2} - I_{+, k+y_2}\right) 10^{-8} \frac{1000}{hc}$$
(10.114)

Example 10.14.

 $I = 12 \text{ W m}^{-2} \text{ in band } 0.495 \text{ }\mu\text{m} < -0.505 \text{ }\mu\text{m}$ 

---> mean =  $0.5 \ \mu m$ 

---> 
$$I_{p}$$
, = 3.02 x 10<sup>15</sup> photons cm<sup>-2</sup> s<sup>-1</sup>