
Hybrid Estimation for Unmanned Aircraft Systems Detect and Avoid

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Motivation

- Airspace integration for Unmanned Aircraft Systems (UAS) flights beyond vision line of sight
- Replace pilot vision functionality through appropriate sensors
- The need for Detect and Avoid (DAA): UAS must be able to identify the non-cooperative intruder aircraft for integration into National Airspace System (NAS)
 - Certifiable DAA sensors

Motivation

- RTCA MOPS (Radio Technical Commission for Aeronautics - Minimum Operational Performance Standards) – Phase II^[1]
 - Extended requirements for UAS operation, much larger scope through different airspace classes
 - Sensors and architectures to enable DAA equipment to be installed on a wider range of UAS (Phase 1 focused on large high-performance UAS)
- Analyze operations and encounters of smaller UAS at low altitude
 - Allow the use of airborne non-cooperative sensors (no ADS-B) and with less performance than the Phase 1 Air-to-Air Radar (new MOPS for Electro-Optical sensors)

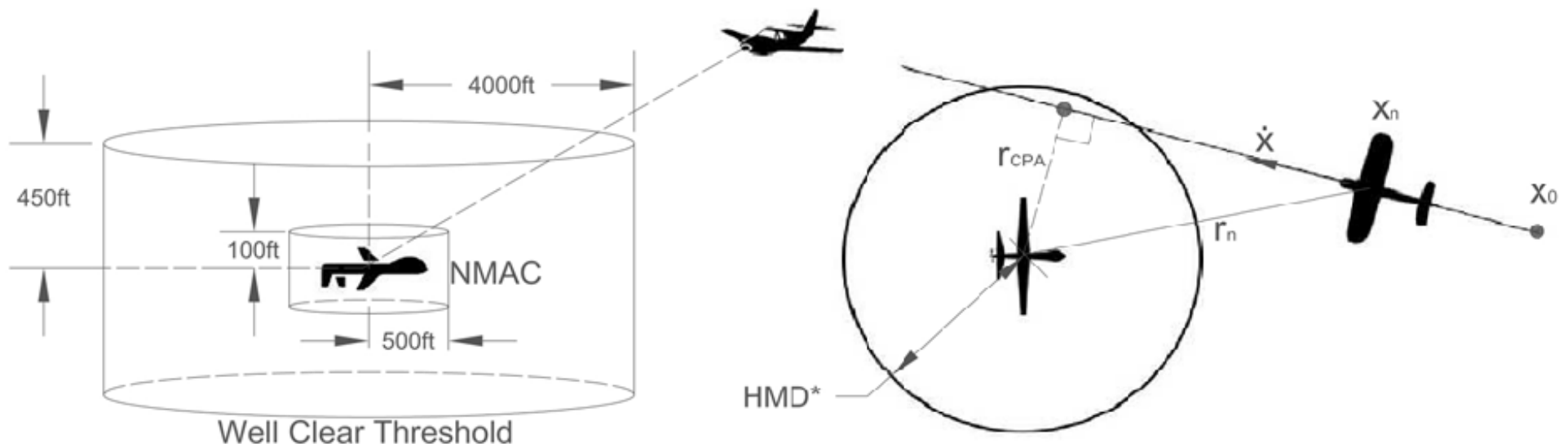
[1] Detect and Avoid (DAA) DRAFT White Paper Phase 2 (RTCA Paper No. 144-17/SC228-051) - June 5, 2017

Contributions/Objectives

- Develop new methods to apply safety standards in Detect and Avoid (DAA) functions with a maneuvering intruder
 - Advance previous work that have used linear predefined trajectories
 - Generate random trajectories using an established Encounter Model
 - Target Tracking
 - Multiple Model Adaptive Estimation (MMAE)
 - Interactive Multiple Model (IMM)
 - **Hazard States Error Analysis** using the IMM
 - **New method** for Closest Point of Approach (CPA) estimation based on the IMM prediction

Self-Separation

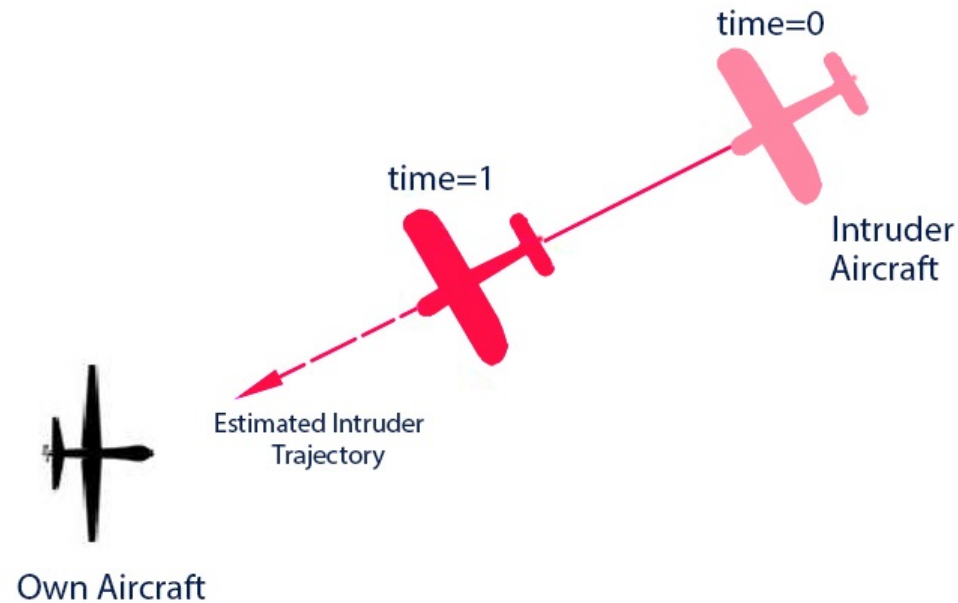
- Self-separation: visual requirement to remain well clear^[2]
 - Well clear threshold (WCT) definition (RTCA SC-228)^[3]:
 - Time to horizontal closest point of approach (CPA): $\tau = 35s$
 - Horizontal miss distance of 4000ft and vertical miss distance of 450ft



[2] 14 CFR 91.113

[3] RTCA SC-228, Draft DAA MOPS, V3.3, Apr 2016

Target Tracking



- Our own aircraft has to detect and estimate the intruder aircraft trajectory
- Uncertainty in the measurement due to estimation error
 - As the DAA sensors gets more measurements, our estimated trajectory error decreases

Target Tracking

- Tracking maneuvering targets
- Two main difficulties:
 - Measurement uncertainty (sensor noise)
 - Unknown intruder aircraft intent
- A potential solution is a Kalman filter (KF)
 - Limited in performance for such problems
 - Single motion model
 - Response to dynamics changes as the target maneuvers

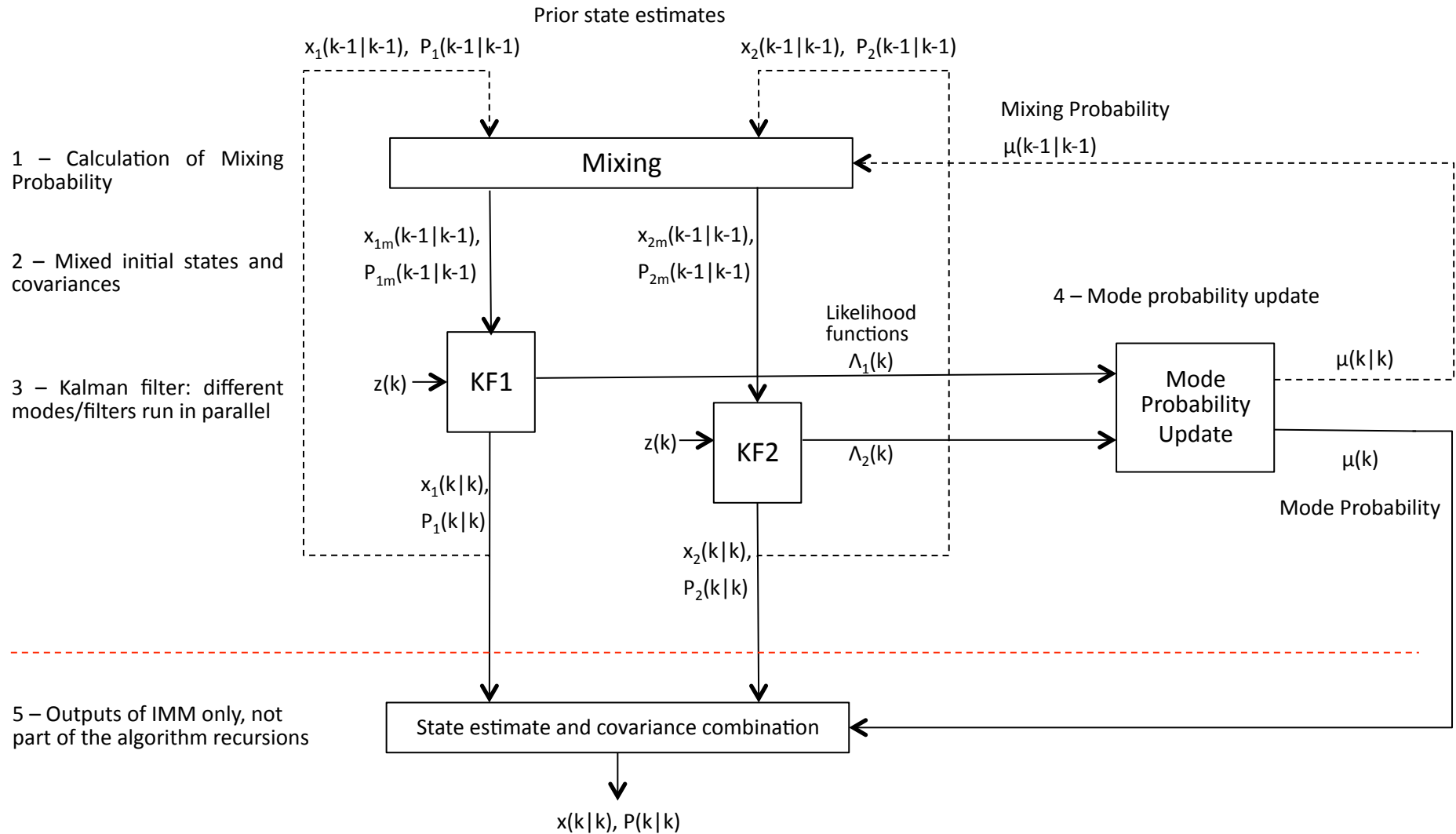
Multiple Model Approach

- Another alternative is the Multiple Model Adaptive Estimation (MMAE) for state estimation
 - Account for different target behavior
 - It is assumed that the system obeys one of a finite number of dynamic models
 - Multiple filters (running in parallel) estimate the states of targets with changing dynamics
- These systems are called hybrid
 - Continuous dynamics
 - Discrete mode changes (multiple model)

IMM Algorithm

- Optimal MMAE estimation: must account for any potential estimation history
 - Would require r^k filters (estimation histories) for r modes and k epochs
- The Interactive Multiple Model (IMM) algorithm
 - State estimate is computed under each possible current model using r filters
 - Each filter uses a different combination of the previous estimates
 - Mixed initial conditions
 - Target dynamics modeled with simple kinematics (corresponding to an individual mode)
- Typically, IMM is a good compromise between complexity and performance, ^[4] to be evaluated in our specific problem

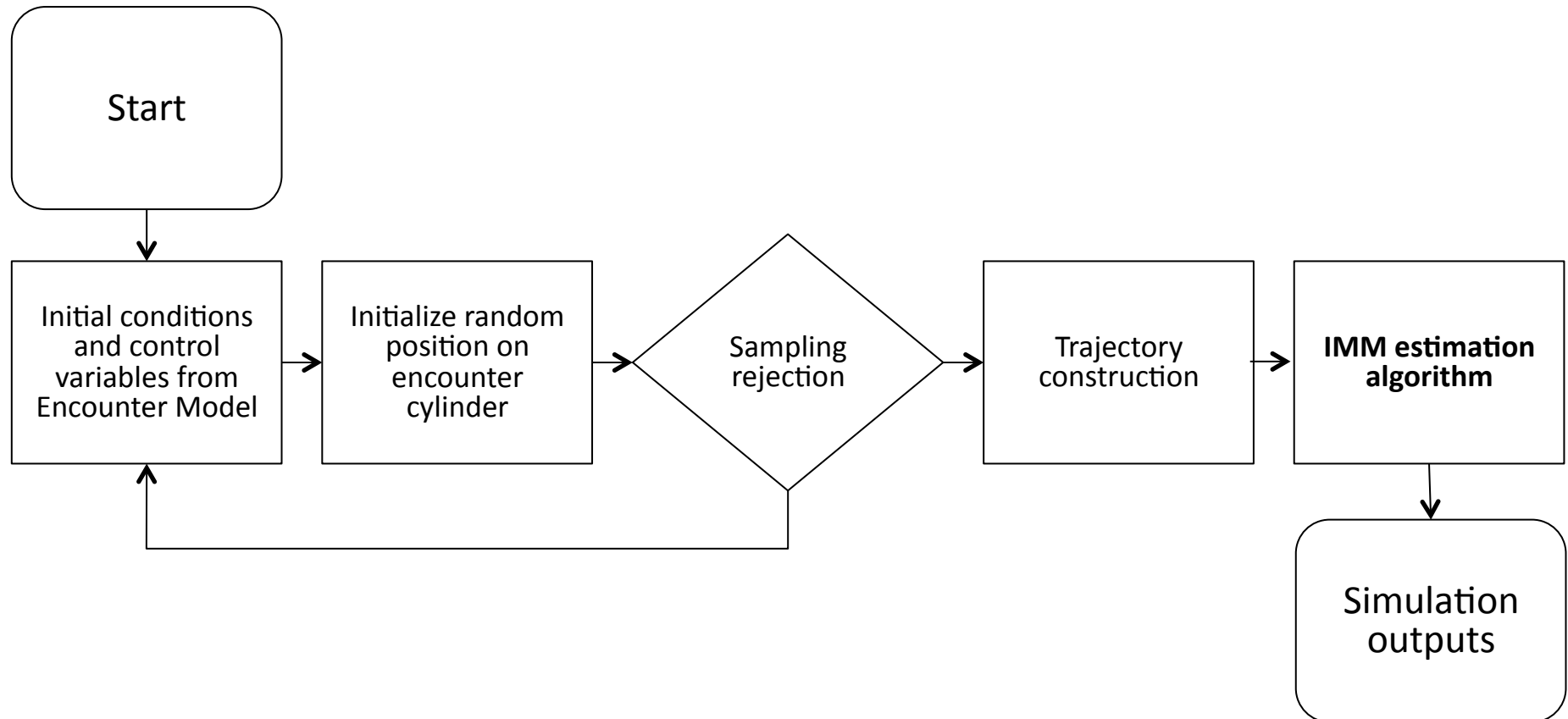
IMM Algorithm



Encounter Model - Overview

- How do we define intruder trajectories for the IMM analysis
- Another tool that we are using is an encounter model
 - Simulations that can represent realistic trajectories
 - They are generated with the same likelihood as found in real aircraft trajectories
- MIT Lincoln Lab Encounter Model: based on US radar data ^[5]
 - Trajectory construction is not provided with the encounter model
 - The initial conditions do not specify position or direction of velocity
 - It gives as output initial conditions and control variables for each time step

Simulation Steps



- At the encounter cylinder, start position and angle:
 - The encounter cylinder is assumed to have $\pm 3000\text{ft}$ height^[10]/ 5.5 NM radius
 - Intruder aircraft starts at a random position at the encounter cylinder surface, at a random heading angle

[10] RTCA SC-228, Draft DAA MOPS, V3.3, Apr 2016

- Based in an ATC scenario^[7,8,9], the motions of an aircraft can be summarized as ascent/descent, straight level flight, turning, and change of speed
 - Mode 1 - Constant Velocity
 - Mode 2 - Constant Velocity 3D (non-zero \dot{h})
 - Mode 3 - Coordinated Turn
 - Mode 4 - Coordinated Turn 3D (non-zero \dot{h})
 - Mode 5 - Constant Linear Acceleration
 - Mode 6 - Constant Linear Acceleration 3D (non-zero \dot{h})

[7] Kochenderfer, M., et al., Uncorrelated Encounter Model of the NAS. Project Report ATC-345, MIT Lincoln Lab, 2008

[8] Li, X. R., & Bar-Shalom, Y. (1993). Design of an interacting multiple model algorithm for air traffic control tracking. IEEE Transactions on Control Systems Technology, 1(3), 186–194

[9] Bar-Shalom, Y., Kirubarajan, T., & Li, X. (2007). Estimation with applications to tracking and navigation:. New York, NY: Wiley

IMM - Transition Matrix

- Transition Matrix of the Markov Chain (M_{ij}) – used on the mode probability update - is based on Encounter Model runs (10^6), with 1 second timesteps
 - Homogeneous Markov Chain: time-invariant

$$M_{ij} = \begin{bmatrix} 0.98038 & 0.00692 & 0.00562 & 0.00093 & 0.00508 & 0.00108 \\ 0.02536 & 0.96022 & 0.00246 & 0.00509 & 0.00200 & 0.00487 \\ 0.03263 & 0.00280 & 0.95063 & 0.00646 & 0.00624 & 0.00123 \\ 0.01280 & 0.01891 & 0.01456 & 0.94566 & 0.00172 & 0.00636 \\ 0.02551 & 0.00250 & 0.01098 & 0.00077 & 0.95314 & 0.00710 \\ 0.00926 & 0.01860 & 0.00204 & 0.01147 & 0.01049 & 0.94814 \end{bmatrix}$$

- The mode probability initial values:

$$\mu_{ip} = \begin{bmatrix} 0.55117 & 0.15393 & 0.10708 & 0.04781 & 0.09292 & 0.04709 \end{bmatrix}$$

Hazard States

- At the definition of the Hazard States in the **DAA MOPS**
 - Calculation of the CPA is time based

$$CPA = \sqrt{(d_x + v_{rx}t_{CPA})^2 + (d_y + v_{ry}t_{CPA})^2}$$

$$t_{CPA} = \max\left(0, -\frac{d_x v_{rx} + d_y v_{ry}}{v_{rx}^2 + v_{ry}^2}\right)$$

where: $v_{rx} = \dot{x}_2 - \dot{x}_1$ is the relative horizontal velocity in the x dimension

$v_{ry} = \dot{y}_2 - \dot{y}_1$ is the relative horizontal velocity in the y dimension

$d_x = x_2 - x_1$ is the current horizontal separation in the x dimension

$d_y = y_2 - y_1$ is the current horizontal separation in the y dimension

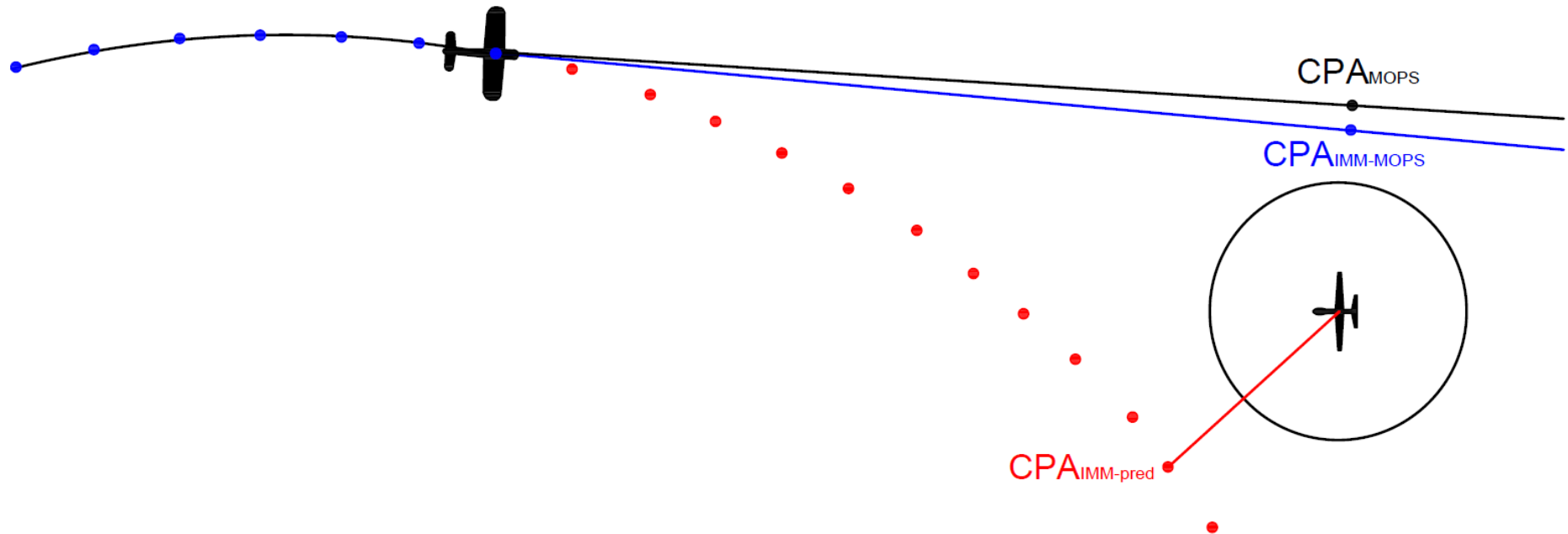
- Vertical separation for alerting performance requirements are based on actual altitudes
 - We assume constant vertical velocity to account for the lookahead time alert criteria

CPA Calculation

- In order to minimize prediction errors on the Hazard States, we introduce a new method instead of using the MOPS calculations (which are based on a linear trajectory propagation)
 - Use Kalman prediction step as estimation for CPA (**IMM Prediction**)
- There will be four main different **CPA definitions**:
 - **MOPS**: using the formula as defined by the MOPS
 - **IMM-MOPS**: using the formula as defined by the MOPS and the best trajectory estimation by the IMM
 - **IMM-Predicted**: estimated closest point of approach calculated at each timestep, using the IMM prediction (new method)
 - **True**: only known after the simulation has ended (influenced by future mode switches)

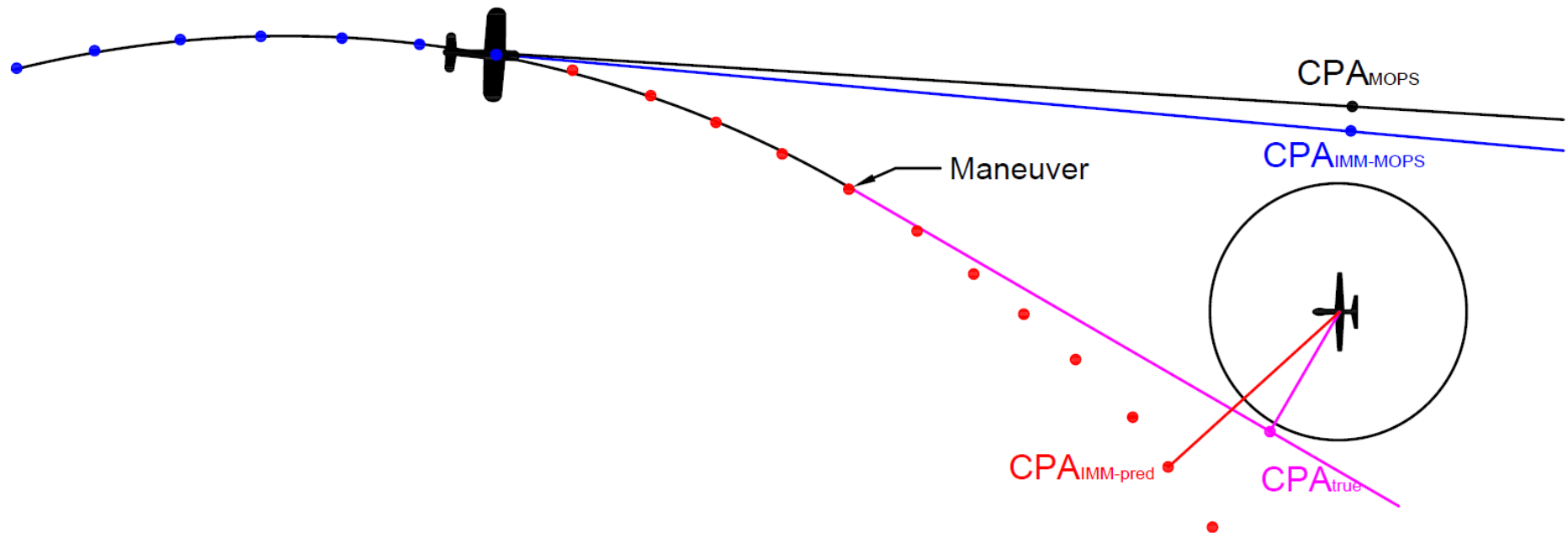
IMM Prediction

- Under maneuvers, the Hazard States estimation will be changing at each timestep



IMM Prediction

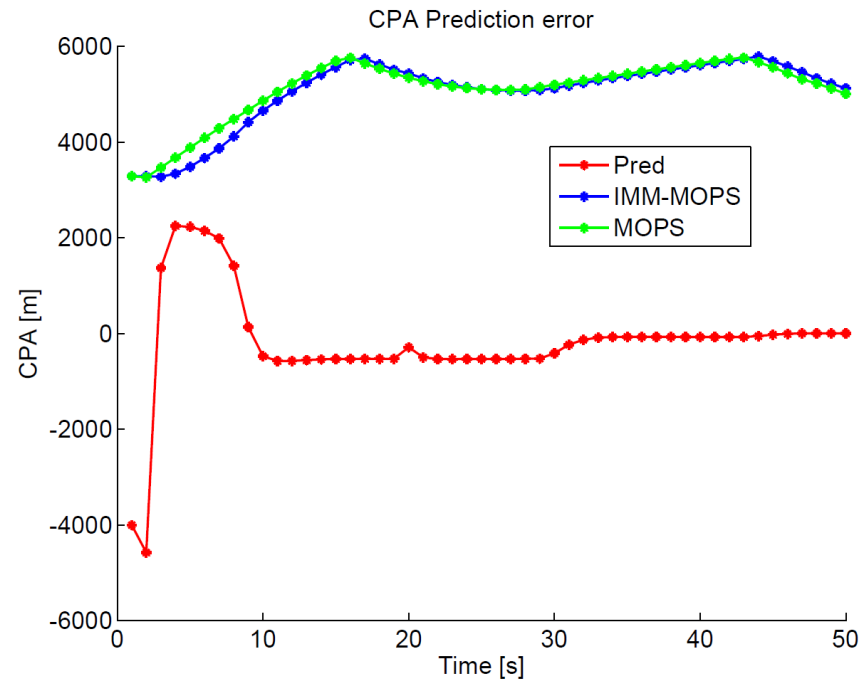
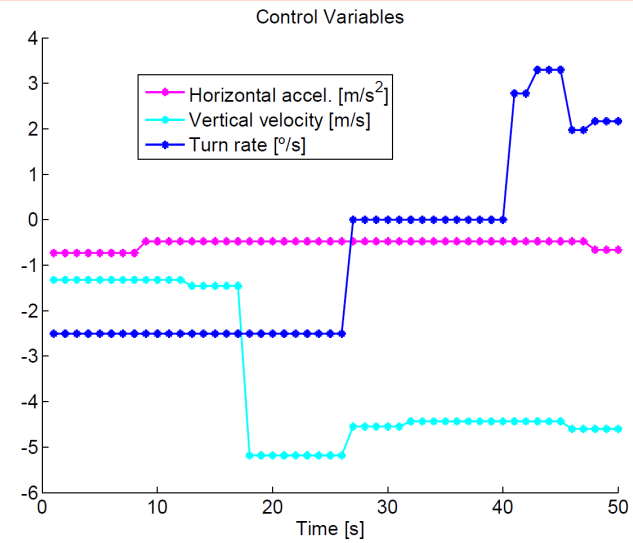
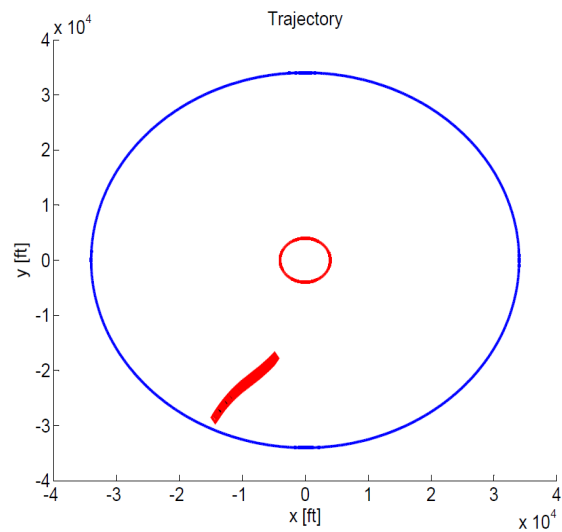
- We don't know future aircraft intent (maneuver changes)
 - Using the knowledge of the current maneuver can improve our estimation
 - Our estimation will get better as the IMM recognizes the maneuver



Simulation

- Own aircraft: linear trajectory, constant velocity of 200kt
- Intruder aircraft: randomly generated by the encounter model
- Simulation time: 50s / sample rate: 1Hz
- Zero *sensor noise*

IMM Prediction - Results



IMM Prediction - Discussion

- The estimation get better after the IMM recognizes the maneuver and adapts to the new predictions
- The overall prediction error when compared to the True CPA is considerably reduced using the new method
- Use the Encounter Model together with these tools for a safety evaluation
 - Based on the NMAC/LoWC probability associated with the encounter rate

$$P(LoWC) = \lim_{N_s \rightarrow \infty} \sum_{j=1}^{N_s} P(LoWC|E_j)$$

$$\lambda_{enc} = \rho \bar{V}$$

$$\lambda_{LoWC} = P(LoWC)\lambda_{enc}$$

Summary

- Developing new tools for evaluate a DAA system performance with a maneuvering intruder
 - Define system requirements
- In this work, we investigated an intruder dynamics estimation method using an Interactive Multiple Model approach
 - Using an established encounter model to generate trajectories which include maneuvering intruders in proportion of their likelihood of occurrence
- Developed a new method for Hazard States estimation based on the IMM prediction

- Future research:
 - Further analysis on the error sources (*mode transition adaptation; mode transition prediction; modeling error; sensor noise*)
 - Considerations with respect to Field of Regard from the MOPS^[11]
 - ± 110 with respect to the longitudinal axis
 - ± 15 vertically referenced to the flight path
 - Safety evaluation based on the NMAC/LoWC probability associated with the encounter rate

Thank you!

Questions?

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