An Eulerian approach for the simulation of soft solids in fluids

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Results

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Introduction and Motivation

- System of soft solids in a fluid are ubiquitous
 - Animal tissues, cell membrane.
- Studied for decades arbitrary Lagrangian-Eulerian (ALE) method - Stiff solids.
- Need for a fully Eulerian approach with "true solid constitutive laws".
 - Eulerian Godunov method (Miller & Colella 2001) unbounded domains
 - Reference Map Technique (RMT) (Kamrin et al. 2012)





Reference Map Technique



Reference map

$$\begin{split} \vec{\xi}(\vec{x},t) &= \vec{X} \\ \frac{D\vec{\xi}(\vec{x},t)}{Dt} &= 0 \qquad \Rightarrow \qquad \frac{\partial\vec{\xi}(\vec{x},t)}{\partial t} + \vec{u}.\vec{\nabla}\vec{\xi}(\vec{x},t) = 0 \end{split}$$

Deformation gradient

$$\mathbb{F}(\vec{X},t) = \partial \vec{x} / \partial \vec{X} = (\overrightarrow{\nabla} \overrightarrow{\xi} (\vec{x},t))^{-1}$$

[Valkov et al., J. Appl. Mech., 82, 2015].

Governing equations for solids and fluids

Momentum balance

$$\frac{\partial(\rho\vec{u})}{\partial t} + \nabla .(\rho\vec{u}\otimes\vec{u}) = \nabla .\underline{\underline{\sigma}}$$

Mass balance

Fluid:

$$\frac{\partial \rho}{\partial t} + \vec{\nabla}.(\vec{u}\rho) = 0 \qquad \Rightarrow \qquad \vec{\nabla}.\vec{u} = 0$$

Solid:

$$\rho = \rho_o(\det(\mathbb{F}))^{-1} \qquad \Rightarrow \qquad \det(\mathbb{F}) = 1$$

Cauchy stress

Newtonian fluid:

$$\underline{\underline{\sigma}}^{f} = \mu \left[\left(\vec{\nabla} \vec{u} \right) + \left(\vec{\nabla} \vec{u} \right)^{T} \right] - \mathbb{1} \left(\vec{\nabla} P \right)$$

Neo-Hookean solid:

$$\underline{\underline{\sigma}}^{s} = 2(det\mathbb{F})^{-1}\mathbb{F}\frac{\partial\psi(\mathbb{C})}{\partial\mathbb{C}}\mathbb{F}^{T}$$
$$\hat{\psi}(\mathbb{C}) = \mu[tr\mathbb{C}-3] \quad \Rightarrow \quad \underline{\underline{\sigma}}^{s} = 2\mu^{s}[(\vec{\nabla}\vec{\xi})^{T}(\vec{\nabla}\vec{\xi})]^{-}$$



 $\vec{\xi}$ defined only within the solid.





Procedure:

• Solve for $\vec{\xi}_{n+1}$ in Ω_S .





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- Compute $\underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f$.



Basic methodology

- Solve for $\vec{\xi}_{n+1}$ in Ω_S .
- $\vec{\xi}_{n+1} \rightarrow \text{Extrapolate outside } \Omega_S$.
- $\vec{\xi}_{n+1} \rightarrow \text{Construct } \phi \rightarrow \text{Construct } H(\phi).$
- Compute $\underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f$.
- $\underline{\underline{\sigma}} \leftarrow \text{Blend} \ f(H(\phi), \underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f)$
- $\underline{\underline{\sigma}} \rightarrow \text{Compute } \vec{u} \rightarrow \text{Project } \vec{\nabla}.\vec{u} = 0.$







Level-set reconstruction

Analytical expression for $\phi(\vec{x}, t = 0)$ is known.

Level-set reconstruction

$$\phi(\vec{x},t)=\phi(\vec{\xi},t=0)$$

Reinitialize ϕ using Fast-marching method.

Closure model

 $\label{eq:solid} Fluid-Solid\ coupling\ is\ based\ on\ the\ ``one-fluid\ formulation".$

Smoothed heaviside function			
(0	$x \leq -w_T$	
$H(x) = \begin{cases} \frac{1}{2} \left(1 + \frac{x}{w_T} + \frac{1}{\pi}\right) \\ \frac{1}{2} \left(1 + \frac{x}{w_$	$\frac{1}{\pi}sin(\frac{\pi x}{w_T}))$	$ x < w_T$	
l	1	$x \ge w_T$	

constructed based on the reinitialized level-set field.

Mixture model

$$\underline{\underline{\sigma}} = H(\phi(\vec{x}, t))\underline{\underline{\sigma}}^f + (1 - H(\phi(\vec{x}, t)))\underline{\underline{\sigma}}^s$$

$$\rho = H(\phi(\vec{x},t))\rho^f + (1-H(\phi(\vec{x},t)))\rho^s$$

Capability to handle Solid-solid and solid-wall contact.

Updates and major issues fixed

• Momentum conservation - conservative form of equations.

$$\frac{\partial \rho \vec{u}}{\partial t} + \vec{\nabla}.(\rho \vec{u} \vec{u}) = \vec{\nabla}.(\sum_i \underline{\underline{\sigma}}_i)$$

- Non-dissipative schemes stress evaluation, convective flux evaluation.
 - Central difference schemes
 - No viscous damping in the solid
- Modified reference map equation momentum consistent solid advection.
 - Improved robustness

$$\frac{\partial \vec{\xi}(\vec{x},t)}{\partial t} + H(\psi)\vec{u}.\vec{\nabla}\vec{\xi}(\vec{x},t) = 0$$

- Least-squares based extrapolation method.
- Collocated grid.

[Jain & Mani, CTR Annual Research Briefs, 2017]

Least-square method for extrapolation



	PDE	least-squares
Error (L_2)	$ 8.32 \times 10^{-4}$	6.72×10^{-9}
Cost	$\approx 1550 \mathrm{ms}$	$\approx 100 \mathrm{ms}$





Lid-driven cavity

• Re = 1000

• 100x100 grid.



Problems with the previous approach



Two solids in a Taylor-Green Vortex



Modified reference map advection equation

$$\frac{\partial \vec{\xi}(\vec{x},t)}{\partial t} + H(\psi)\vec{u}.\vec{\nabla}\vec{\xi}(\vec{x},t) = 0$$

Simulations of a solid in a fluid with wall contact

Collision in microgravity:



Collision in gravity - Stiff solid:



Collision in gravity - Soft solid:



Conservative vs Non-conservative formulation



Initial state

Non-conservative formulation:



Conservative formulation:



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Conclusion

We here presented:

- An incompressible fully Eulerian formulation for soft solids in fluids using an approximate Projection method.
- Advantages:
 - Momentum conserving formulation.
 - Non-dissipative schemes for flux computation better KE conservation.
 - Solid momentum advection is consistent with reference map advection.
 - An accurate and cost effective extrapolation procedure.

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Reference:

Jain, S, S, & Mani, A, 'An incompressible Eulerian formulation for soft solids in fluids', *CTR Annual Research briefs*, 2017.

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