

# FREQUENCY/PHASE MODULATION

GENERALLY CAN FORMULATE AS ANGLE MODULATION

$$v_o(t) = A \cos \theta(t)$$

$$= A \cos(\omega t + \phi)$$

Frequency  $\uparrow$        $\uparrow$  Phase

(FM)

(PM)

Both are important and used in practice, let's do FM first.

$$\omega \equiv \frac{d\theta}{dt} \quad (\text{a})$$

Instantaneous frequency is

$$f = f_c + K_o v_m(t) \quad (\text{b})$$

Equating (a) & (b) above

$$\frac{d\theta}{dt} = 2\pi f_c + 2\pi K_o v_m(t)$$

And then integrating w.r.t. time

$$\theta(t) = 2\pi f_c t + \theta_o + 2\pi K_o \int v_m(t) dt$$

$$\text{Assuming } v_m(t) = v_p \cos(2\pi f_m t)$$

(and letting  $\theta_o + \text{integration const.} \equiv 0$ )

$$\theta(t) = 2\pi f_c t + \frac{\overbrace{K_o v_p}^{\Delta f_c}}{f_m} \sin(2\pi f_m t)$$
$$m_f \equiv \frac{K_o v_p}{f_m}$$

$$v_o(t) = A \cos \left( \underbrace{2\pi f_c t}_a + \underbrace{m_f \sin(2\pi f_m t)}_b \right)$$

Narrow -- vs. wide - Band FM

NBFM  $m_f < 0.25$  (quarter radian)

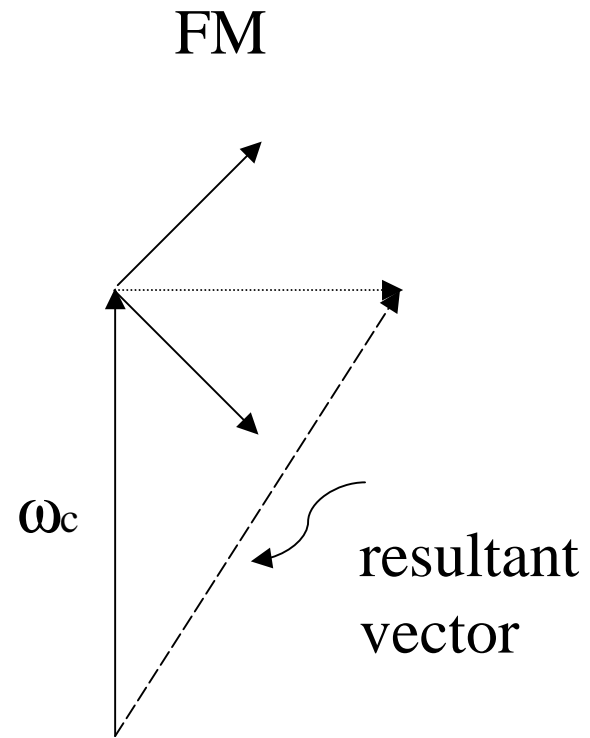
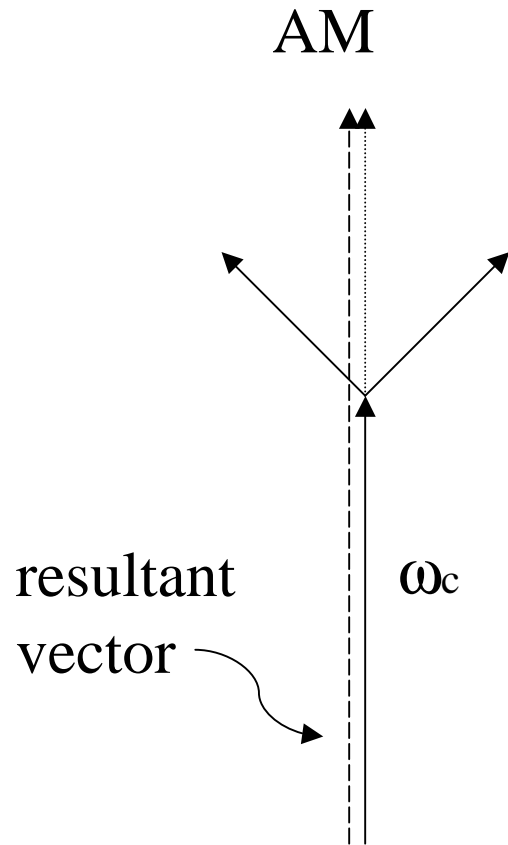
$$A \cos(a + b) \equiv A(\cos b \cos a - \sin b \sin a)$$

$$v_{out}(t) = A[\cos(m_f \sin \omega_m t) \cos \omega_c t - \sin(m_f \sin \omega_m t) \sin \omega_c t]$$

For NBFM using small  $\angle$  formulae  $\cos(x) \simeq 1$ ,  $\sin(x) \simeq x$

$$v_o(t) = A[\cos \omega_c t - m_f \sin \omega_m t \sin \omega_c t]$$

Wow, looks like AM (...sort of...)

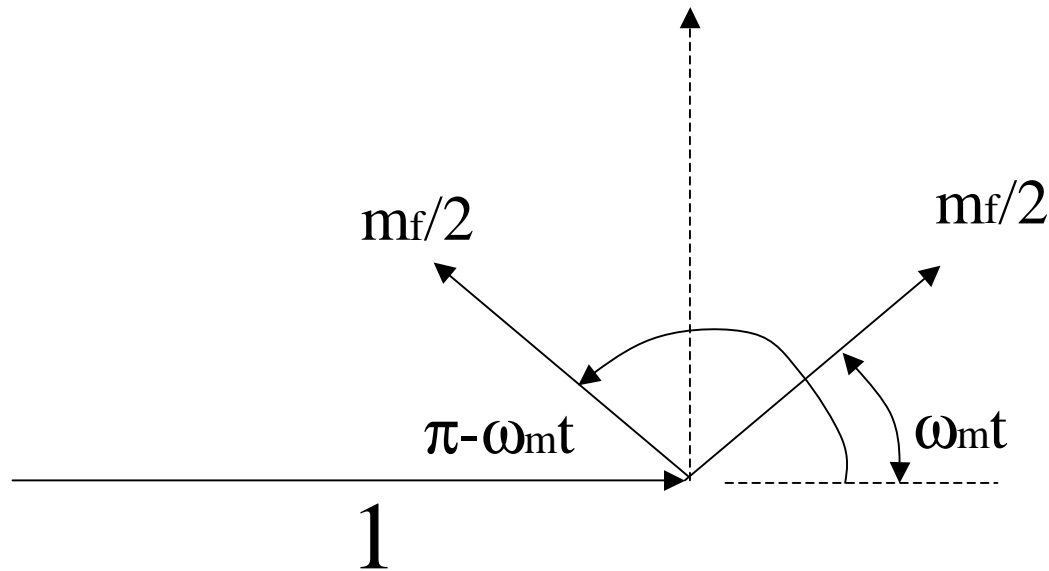


Actually, getting quantitative about these two figures:

$$v_o|_{FM}(t) = \cos \omega_c t - \frac{m_f}{2} [\cos(\omega_c - \omega_m)t - \cos(\omega_c + \omega_m)t]$$

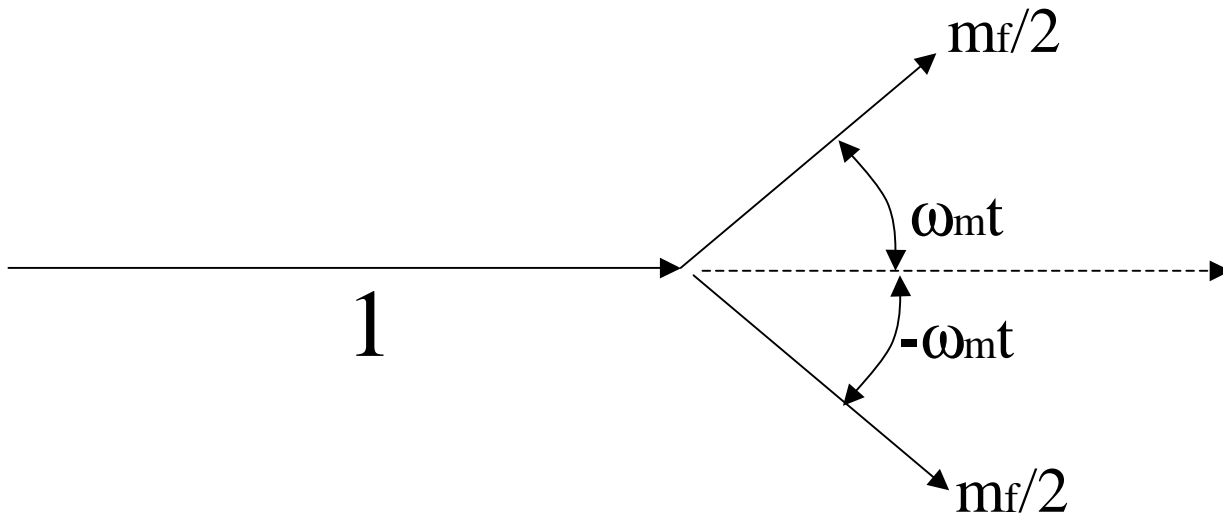
$$= R_e \left[ e^{j\omega_c t} \left( 1 - \frac{m_f}{2} e^{-j\omega_m t} + \frac{m_f}{2} e^{+j\omega_m t} \right) \right]$$

$((-)) \equiv \text{shift by } +\pi$



$$v_o|_{AM}(t) = \cos \omega_c t + \frac{m_f}{2} [\cos(\omega_c + \omega_m)t + \cos(\omega_c - \omega_m)t]$$

$$= R_e \left[ e^{j\omega_c t} \left( 1 + \frac{m_f}{2} e^{j\omega_m t} + \frac{m_f}{2} e^{-j\omega_m t} \right) \right]$$



WBFM (or just FM with  $m_f > 0.25$ )

$$\begin{aligned}v_o(t) &= \sin(\omega_c t + m_f \sin \omega_m t) \\ &= \sin \omega_c t \cos(m_f \sin \omega_m t) + \cos \omega_c t \sin(m_f \sin \omega_m t)\end{aligned}$$

Without using small angles...Bessel Functions!

$$\begin{aligned}v_o|_{WBFM}(t) &= J_0(m_f) \sin \omega_c t + \\ &2J_1(m_f) \cos \omega_c t \sin \omega_m t + \\ &2J_2(m_f) \sin \omega_c t \cos 2\omega_m t + \\ &2J_3(m_f) \cos \omega_c t \sin 3\omega_m t + \dots\end{aligned}$$

## The attached pages give:

- Table\* of Bessel Function values as a function of  $m_f$
- A graphical version of the data\*
- An example of what the resultant "vector diagram\*" looks like for  $m_f=1$

### Comments:

- The J's are higher order terms (harmonics beyond  $\omega_c \pm \omega_m$ )
- This is wide band (WBFM) and hence  $\beta$  gets larger ( $m_f > 0.25$ )

\*Figures from Chapter 9, book by P.H. Young, Electronic Communication Techniques, 1990, Merrill/Macmillan Publishing

Bessel functions are solutions of the Bessel equation:

$$x^2 y'' + xy' + (x^2 - p^2)y = 0$$

$$J_0(x) = \sum_0^{\infty} (-1)^k \frac{x^{2k}}{2^{2k} (k!)^2}$$

$$J_1(x) = \sum_0^{\infty} (-1)^k \frac{x^{2k+1}}{2^{2k+1} k!(k+1)!}$$

$$J_{n+1}(x) = \frac{2n}{x} J_n(x) - J_{n-1}(x)$$

Related formulations for trigonometric functions

$$\cos(m \cos x) = J_0(m) + 2 \sum_{k=1}^{\infty} (-1)^k J_{2k}(m) \cos(2kx)$$

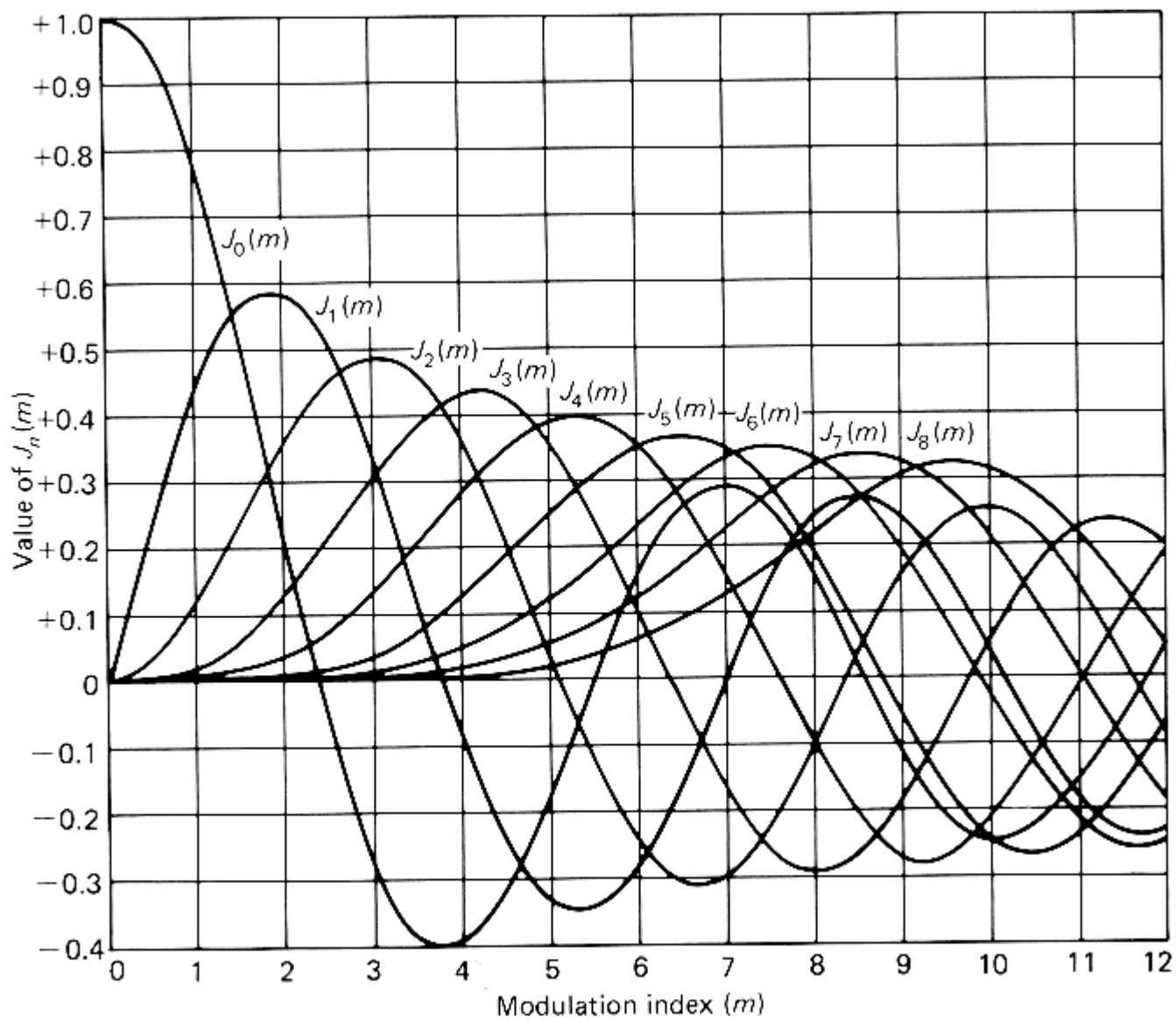
$$\cos(m \sin x) = J_0(m) + \sum_{k=1}^{\infty} J_{2k}(m) \cos(2kx)$$

$$\sin(m \cos x) = 2 \sum_{k=1}^{\infty} (-1)^k J_{2k+1}(m) \cos(2k+1)x$$

$$\sin(m \sin x) = 2 \sum_{k=0}^{\infty} J_{2k+1}(m) \sin(2k+1)x$$

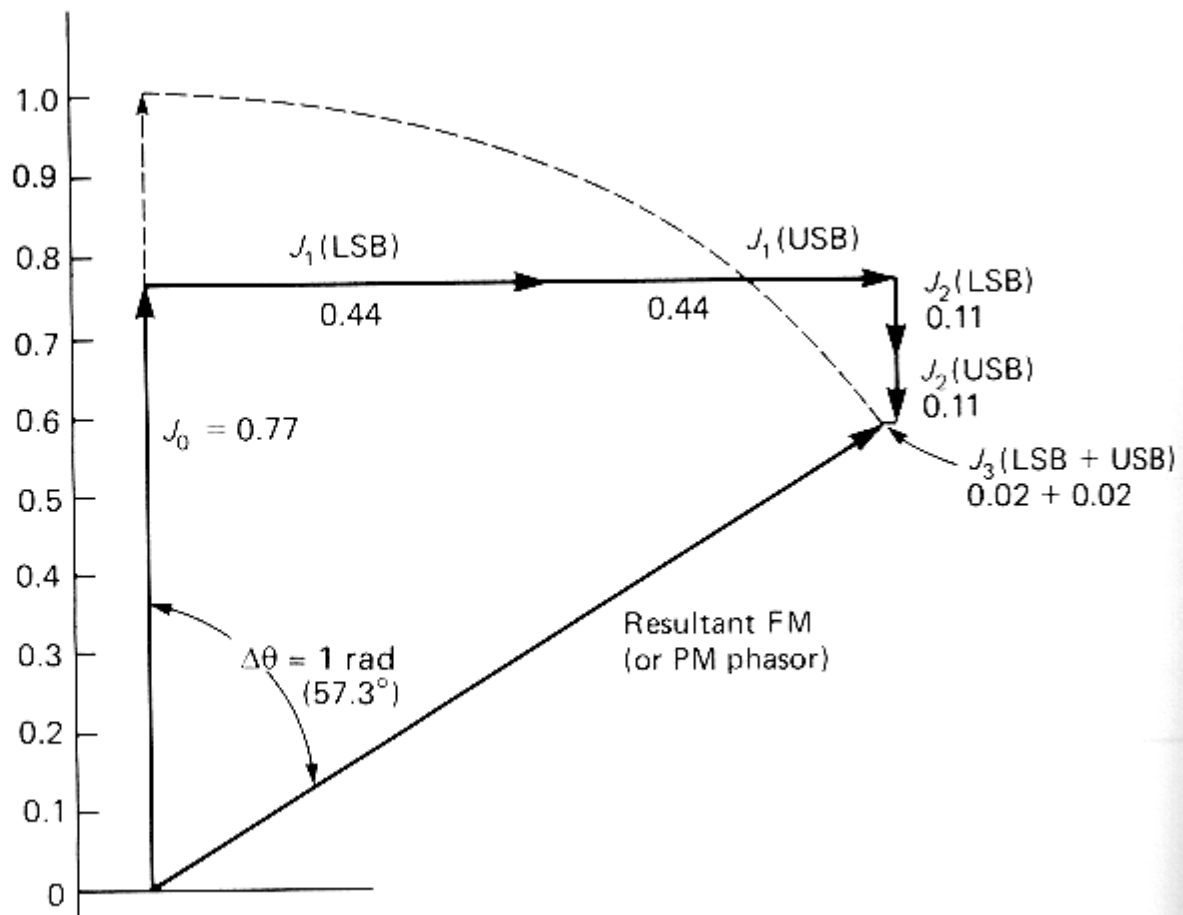
**TABLE 9-1** Bessel Functions of the First Kind,  $J_n(m_f)$

$m_f$	$J_0$	$J_1$	$J_2$	$J_3$	$J_4$	$J_5$	$J_6$	$J_7$	$J_8$	$J_9$	$J_{10}$	$J_{11}$	$J_{12}$	$J_{13}$	$J_{14}$
0.00	1.00	—	—	—	—	—	—	—	—	—	—	—	—	—	—
0.25	0.98	0.12	—	—	—	—	—	—	—	—	—	—	—	—	—
0.5	0.94	0.24	0.03	—	—	—	—	—	—	—	—	—	—	—	—
1.0	0.77	0.44	0.11	0.02	—	—	—	—	—	—	—	—	—	—	—
1.5	0.51	0.56	0.23	0.06	0.01	—	—	—	—	—	—	—	—	—	—
2.0	0.22	0.58	0.35	0.13	0.03	—	—	—	—	—	—	—	—	—	—
2.4	0	0.52	0.43	0.20	0.06	0.02	—	—	—	—	—	—	—	—	—
2.5	-0.05	0.50	0.45	0.22	0.07	0.02	0.01	—	—	—	—	—	—	—	—
3.0	-0.26	0.34	0.49	0.31	0.13	0.04	0.01	—	—	—	—	—	—	—	—
4.0	-0.40	-0.07	0.36	0.43	0.28	0.13	0.05	0.02	—	—	—	—	—	—	—
5.0	-0.18	-0.33	0.05	0.36	0.39	0.26	0.13	0.05	0.02	—	—	—	—	—	—
6.0	0.15	-0.28	-0.24	0.11	0.36	0.36	0.25	0.13	0.06	0.02	—	—	—	—	—
7.0	0.30	0.00	-0.30	-0.17	0.16	0.35	0.34	0.23	0.13	0.06	0.02	—	—	—	—
8.0	0.17	0.23	-0.11	-0.29	-0.10	0.19	0.34	0.32	0.22	0.13	0.06	0.03	—	—	—
9.0	-0.09	0.25	0.14	-0.18	-0.27	-0.06	0.20	0.33	0.31	0.21	0.12	0.06	0.03	0.01	—
10.0	-0.25	0.05	0.25	0.06	-0.22	-0.23	-0.01	0.22	0.32	0.29	0.21	0.12	0.06	0.03	0.01



**FIGURE 9-5** Amplitudes of carrier and sidebands for FM (and PM) relative to the unmodulated carrier.

**FIGURE 9-7** Carrier and sidebands add up to transmitted FM (or PM) phasor.



## Phase Modulation

Recall...

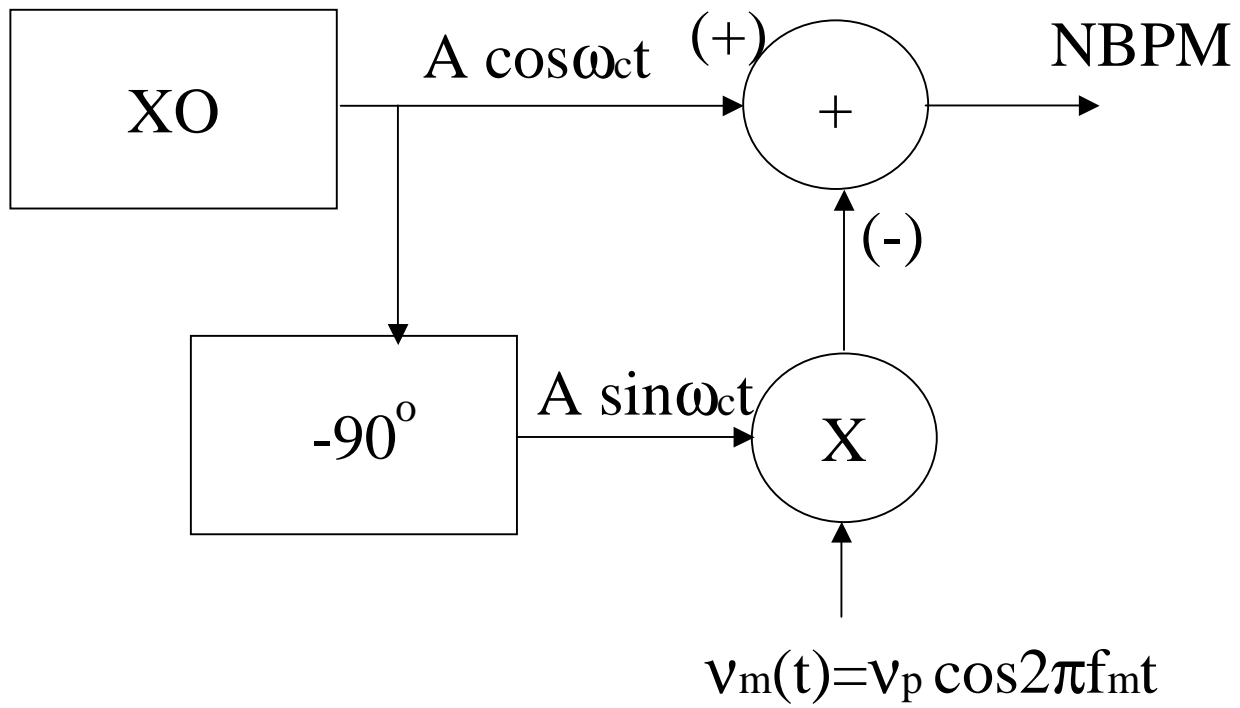
$$v_o(t) = A \cos \theta(t)$$

$\overbrace{(\omega t + \phi)}$

FM      PM

Now, let's go for PM

$$\theta(t) = \omega_c t + K_p v_m(t)$$



$$v_o(t) = A \cos \omega_c t - A(m_p \cos \omega_m t) \sin \omega_c t$$

$$m_p = \Delta\phi = k_p v_p$$

$$\left[ \text{Note : for FM, } m_f = \frac{K_o v_p}{f_m} \right]$$

$\therefore$  for PM constant  $\frac{\omega}{f_m}$  vs. not so with FM]

Also, XO (crystal osc.) can be made super stable with temp. etc. Now the burden of signal processing is to get -90°, mixer etc.