

PROBLEM SET #6

ME III
FALL 2000

6.2

FIND: P_{max}

GIVEN: $2W = 6 \text{ in.}$
 $t = .035 \text{ in.}$

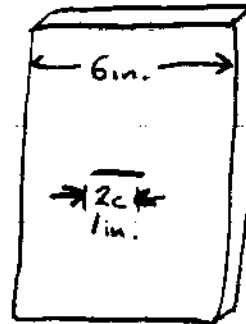
7075-T651A1: $S_u = 78 \text{ ksi}$

$S_y = 70 \text{ ksi}$

central crack: $2c = 1 \text{ in.}$

$K_{Ic} = 60 \text{ ksi}\sqrt{\text{in.}}$

Thin Plate



SOLUTION:

$$K_{Ic} = (1.8\sqrt{c})\sigma_g \quad (6.2)$$

$$\begin{aligned} \sigma_g &= \frac{K_{Ic}}{1.8\sqrt{c}} \\ &= \frac{60 \text{ ksi}\sqrt{\text{in.}}}{1.8(\sqrt{.5 \text{ in.}})} \end{aligned}$$

$$\sigma_g = 47.14 \text{ ksi}$$

$$\begin{aligned} P &= \sigma_g (2wt) \\ &= (47.14 \text{ ksi})(6 \text{ in.})(.035 \text{ in.}) \end{aligned}$$

$$P = 9.90 \text{ kips}$$

$$P_{max} = 9,899 \text{ lb}$$

6.7

FIND: P_{max}

GIVEN: thin plate

$$2w = 8 \text{ in.}$$

$$t = .05 \text{ in.}$$

Material: Leaded beryllium copper

$$S_u = 98 \text{ ksi}$$

$$S_y = 117 \text{ ksi}$$

$$K_{Ic} = 70 \text{ ksi}\sqrt{\text{in}}$$

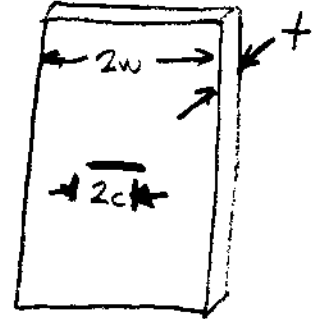
$$2c = 1.5 \text{ in.}$$

SOLUTION: $K_{Ic} = (1.8\sqrt{c})\sigma_g \quad (6.2)$

$$\begin{aligned}\sigma_g &= \frac{K_{Ic}}{1.8\sqrt{c}} \\ &= \frac{70 \text{ ksi}\sqrt{\text{in.}}}{1.8\sqrt{.75 \text{ in.}}} \\ &= 44.91 \text{ ksi}\end{aligned}$$

$$\begin{aligned}P_{max} &= \sigma_g (2wt) \\ &= (44.91 \text{ ksi})(8 \text{ in.})(.05 \text{ in.}) \\ &= 17.96 \text{ kips}\end{aligned}$$

$$P_{max} = 17,962 \text{ lb}$$

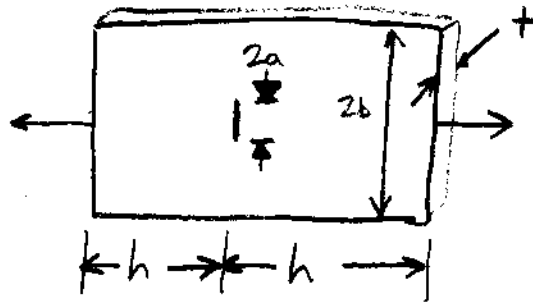


PROBLEM 3

FIND: P_{max} if crack half-length is (a) 10 mm and (b) 24 mm

GIVEN: Material: AISI 1144 Steel
 $K_c = 115 \text{ MPa}\sqrt{\text{m}}$

$b = 40 \text{ mm}$
 $t = 15 \text{ mm}$
 $h = 20 \text{ mm}$
 $N = 3 \leftarrow$ factor of safety



SOLUTION: $N = \frac{K_c}{K}$ $K = \beta \sigma \sqrt{\pi a}$ (from Lecture 16)

① FIND β : PART A: $a/b = .25$ $h/b = .5$ } FROM FIG 5-19 in Lecture 16
 $\beta \approx 1.25$
 PART B: $a/b = .6$ $h/b = .5$ }
 $\beta = 2.5$

② $\sigma = \frac{K}{\beta \sqrt{\pi a}} = \frac{K_c}{N \beta \sqrt{\pi a}}$

(a) $P_{max} = 207.6 \text{ kPa}$
 (b) $P_{max} = 67.0 \text{ kPa}$

$$\frac{P}{2bt} = \frac{K_c}{N \beta \sqrt{\pi a}}$$

$$P = \frac{2bt K_c}{N \beta \sqrt{\pi a}}$$

(a) $P = \frac{(2)(.04 \text{ m})(.015 \text{ m})(115 \text{ MPa}\sqrt{\text{m}})}{(3)(1.25)(\pi \cdot .01 \text{ m})^{\frac{1}{2}}}$

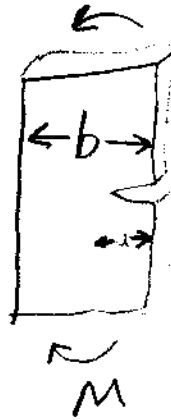
$P_{max} = 207.6 \text{ kPa}$

(b) $P = \frac{(2)(.04 \text{ m})(.015 \text{ m})(115 \text{ MPa}\sqrt{\text{m}})}{(3)(2.5)(\pi \cdot .024 \text{ m})^{\frac{1}{2}}} = 67.0 \text{ kPa}$

PROBLEM 4

FIND: LARGEST EDGE CRACK PERMITTED

GIVEN: $t = 20 \text{ mm}$
 $h = 10 \text{ mm}$
 $M = 10 \text{ N}\cdot\text{m}$
 $N = 2.5$
 $K_c = 3 \text{ MPa}\sqrt{\text{m}}$



SOLUTION: ① FIND σ_g

$$\sigma_g = \frac{My}{I} = \frac{M\left(\frac{b}{2}\right)}{\frac{tb^3}{12}} = \frac{6M}{tb^2}$$

$$= \frac{(6)(10 \text{ N}\cdot\text{m})}{(0.01 \text{ m})(0.02 \text{ m})^2} = 15 \text{ MPa}$$

$$\textcircled{2} \quad K = \beta \sigma_g \sqrt{\pi a}$$

$$\frac{K_c}{N} = \beta \sigma_g \sqrt{\pi a}$$

$$\beta \sqrt{a} = \frac{K_c}{N \sigma_g \sqrt{\pi}} = \frac{(3 \text{ MPa}\sqrt{\text{m}})}{(2.5)(15 \text{ MPa})(\sqrt{\pi})} = .0451$$

③ Make a guess for a , find corresponding β and check against $\beta \sqrt{a} = .0451$

a	β from chart	$\beta \sqrt{a}$
2 mm	$\frac{a}{b} = \frac{2}{10} = .2, \beta = 1.05$.0469 \rightarrow choose smaller a
1 mm	$\frac{a}{h} = \frac{1}{20}, \beta = 1.03$.0323 \rightarrow choose larger a
1.5 mm	$\frac{a}{h} = .075, \beta = 1.06$.0411 \rightarrow choose larger a
1.8 mm	$\frac{a}{h} = .09, \beta = 1.05$.0445 \rightarrow choose larger a
1.85 mm	$\frac{a}{h} = .0925, \beta = 1.04$.045 close enough

$$\boxed{a \approx 1.85 \text{ mm}}$$

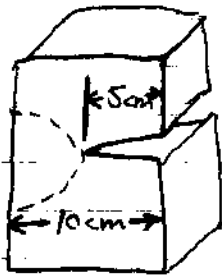
answers might vary slightly due to interpretation of chart.

PROBLEM #6

FIND: Strength of joint as a percentage of strength if the joint were solid as limited by (i) fracture and (ii) fully plastic yielding
 Comment on suitability of steel

GIVEN: (a) $S_y = 550 \text{ MPa}$ $K_c = 55 \text{ MPa}\sqrt{\text{m}}$

(b) $S_y = 400 \text{ MPa}$ $K_c = 200 \text{ MPa}\sqrt{\text{m}}$



SOLUTION: (a) ① FIND a_{eff} ← from lecture 16 notes

$$(i) a_{\text{eff}} = a + \frac{1}{\pi} \left(\frac{K}{S_y} \right)^2 = .05 \text{ m} + \frac{1}{\pi} \left(\frac{55 \text{ MPa}\sqrt{\text{m}}}{550 \text{ MPa}} \right)^2$$

$$[a_{\text{eff}} = \cancel{.05318} \text{ m} \quad .05318]$$

$$\sigma = \frac{K}{\beta \sqrt{\pi a_{\text{eff}}}}$$

$$\beta = 1.5 \leftarrow (a/b = .5 \quad h/b = \infty) \text{ from fig 5-22}$$

~~$$\sigma = \frac{55 \text{ MPa}\sqrt{\text{m}}}{1.5 \sqrt{\pi \cdot .05318 \text{ m}}}$$~~

$$= \frac{55 \text{ MPa}\sqrt{\text{m}}}{1.5 (\pi \cdot .05318)^{.5}} = 89.7 \text{ MPa}$$

$$\text{Strength} = \frac{\sigma}{S_y} = \frac{89.7 \text{ MPa}}{550 \text{ MPa}} = 16.3\%$$

$$\boxed{\text{Strength} = 16.3\%}$$

$$(ii) \sigma_{\text{nom}} = \frac{P_{\text{nom}}}{A}$$

$$\sigma_{\text{notch}} = \frac{P_{\text{notch}}}{\frac{1}{2}A}$$

$$\sigma_{\text{nom}} = \sigma_{\text{notch}}$$

$$\frac{P_{\text{nom}}}{A} = \frac{P_{\text{notch}}}{\frac{1}{2}A}$$

$$\frac{P_{\text{notch}}}{P_{\text{nom}}} = \frac{1}{2}$$

$$\boxed{\text{Strength} = 50\%}$$

#6 (continued)

$$\begin{aligned} (b) \quad a_{\text{eff}} &= a + \frac{1}{\pi} \left(\frac{K}{S_y} \right)^2 \\ &= 0.05 \text{ m} + \frac{1}{\pi} \left(\frac{200 \text{ MPa}\sqrt{\text{m}}}{400 \text{ MPa}\sqrt{\text{m}}} \right)^2 \\ &= ~~0.025~~ 0.1296 \end{aligned}$$

Effective crack length is longer than width of plate. The material will ~~not~~ yield before reaching 200°C.

(c) This steel is not suitable for these temperatures.